

FORM PTO-1390  
REV. 2/01T

U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE

ATTORNEY'S DOCKET NUMBER

**TRANSMITTAL LETTER TO THE UNITED STATES  
DESIGNATED/ELECTED OFFICE (DO/EO/US)  
CONCERNING A FILING UNDER 35 U.S.C. 371**

06074.0020

U.S. APPLICATION NO.  
(If known, see 37CFR1.5)**09/914572**

INTERNATIONAL APPLICATION NO.

PCT/CH00/00120

INTERNATIONAL FILING DATE

March 3, 2000

PRIORITY DATE CLAIMED

March 3, 1999

TITLE OF INVENTION

**METHOD AND DEVICE FOR PROCESSING FILAMENT YARN, AND USE OF SAID DEVICE**

APPLICANT(S) FOR DO/EO/US

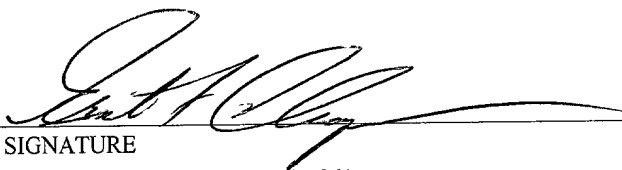
**Patick BUCHMÜLLER**

Applicant(s) herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☐ This is an express request to begin national examination procedures (35 U.S.C. 371(f)). The submission must include items (5), (6), (9) and (21) indicated below.
4. ☒ The US has been elected by the expiration of 19 months from the priority date (Article 31).
5. ☒ A copy of the International Application as filed (35 U.S.C. 371 (c)(2)).
  - a. ☐ is attached hereto (required only if not communicated by the International Bureau).
  - b. ☒ has been communicated by the International Bureau.
  - c. ☐ is not required, as the application was filed with the United States Receiving Office (RO/US).
6. ☒ An English language translation of the International Application as filed (35 U.S.C. 371 (c)(2)).
  - a. ☒ is attached hereto.
  - b. ☐ has been previously submitted under 35 U.S.C. 154 (d)(4).
7. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371 (c)(3)).
  - a. ☐ are attached hereto (required only if not communicated by the International Bureau).
  - b. ☐ have been communicated by the International Bureau.
  - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
  - d. ☒ have not been made and will not be made.
8. ☐ An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371 (c)(3)).
9. ☐ An oath or declaration of the inventor(s) (35 U.S.C. 371 (c)(4)).
10. ☒ An English language translation of the annexes of the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371 (c)(5)).

**Items 11 to 20 below concern document(s) or information included:**

11. ☐ Information Disclosure Statement under 37 CFR 1.97 and 1.98
12. ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. ☐ A **FIRST** preliminary amendment.
14. ☐ A **SECOND** or **SUBSEQUENT** preliminary amendment.
15. ☐ A Substitute specification.
16. ☐ A change of power of attorney and/or address letter.
17. ☐ A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821-1.825.
18. ☐ A second copy of the published international application under 35 U.S.C. 154 (d)(4).
19. ☐ A second copy of the English language translation of the international application 35 U.S.C. 154 (d)(4).
20. ☒ Other items or information:
  - a. ☒ Copy of cover page of International Publication No. WO00/52240
  - b. ☐ Copy of Notification of Missing Requirements.
  - c. ☒ Preliminary Remarks

U.S. APPLICATION NO. (If known, see 37CFR 1.5) <div style="font-size: 1.5em; font-weight: bold;">09/914572</div>		INTERNATIONAL APPLICATION NO. PCT/CH00/00120		ATTORNEY'S DOCKET NUMBER 06074.0020	
21. <input checked="" type="checkbox"/> The following fees are submitted: <b>BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)):</b>  Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO ..... <b>\$1000.00</b>  International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO ..... <b>\$860.00</b>  International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search fee (37 CFR 1.445(a)(2)) paid to USPTO ..... <b>\$710.00</b>  International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4) ..... <b>\$690.00</b>  International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33 (1)-(4) ..... <b>\$100.00</b>  <div style="text-align: right;"><b>ENTER APPROPRIATE BASIC FEE AMOUNT =</b></div>				CALCULATIONS PTO USE ONLY	
Surcharge of \$130.00 for furnishing the oath or declaration later than months from the earliest claimed priority date (37 CFR 1.492 (e)). <div style="float: right;"> <input type="checkbox"/> 20    <input type="checkbox"/> 30         </div>				<div style="text-align: right;">\$</div>	
CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE		
Total Claims	17	- 20 =	x \$18.00	\$	
Independent Claims	3	- 3 =	x \$80.00	\$	
MULTIPLE DEPENDENT CLAIM(S) (if applicable)			+\$270.00	\$270.00	
<b>TOTAL OF THE ABOVE CALCULATIONS =</b>				\$1130.00	
<input type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2.				\$	
<b>SUBTOTAL =</b>				\$1130.00	
Processing fee of <b>\$130.00</b> for furnishing the English translation later than months from the earliest priority date (37 CFR 1.492(f)). <div style="float: right;"> <input type="checkbox"/> 20    <input type="checkbox"/> 30         </div>				<div style="text-align: right;">\$</div>	
<b>TOTAL NATIONAL FEE =</b>				1130.00	
Fee for recording the enclosed assignment (37 CFR 1.21 (h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). <b>\$40.00</b> per property. <div style="text-align: right;">+</div>				<div style="text-align: right;">\$</div>	
<b>TOTAL FEES ENCLOSED =</b>				\$1130.00	
				Amount to be refunded:	\$
				charged:	\$
a. <input checked="" type="checkbox"/> A check in the amount of \$ <u>1130.00</u> to cover the above fees is enclosed. b. <input type="checkbox"/> Please charge my Deposit Account No. _____ in the amount of \$ _____ to cover the above fees. A duplicate copy of this sheet is enclosed. c. <input checked="" type="checkbox"/> The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. <u>06-0916</u> . A duplicate copy of this sheet is enclosed. d. <input type="checkbox"/> Fees are to be charged to a credit card. <b>WARNING:</b> Information on this form may become public. <b>Credit card</b> <b>information should not be included on this form.</b> Provide credit card information and authorization on PTO-2038.					
NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137 (a) or (b)) must be filed and granted to restore the application to pending status.					
<b>SEND ALL CORRESPONDENCE TO:</b> Finnegan, Henderson, Farabow, Garrett & Dunner, L.L.P. 1300 I Street, N.W. Washington, D.C. 20005-3315					
DATED: August 31, 2001				<div style="text-align: center;">           SIGNATURE          Ernest F. Chapman, Reg. No. 25,961          NAME/REGISTRATION NO.       </div>	

FORM PTO-1390  
REV. 2/01T

U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE

**TRANSMITTAL LETTER TO THE UNITED STATES  
DESIGNATED/ELECTED OFFICE (DO/EO/US)  
CONCERNING A FILING UNDER 35 U.S.C. 371**

ATTORNEY'S DOCKET NUMBER

06074.0020

U.S. APPLICATION NO.  
(If known, see 37CFR1.5)**09/914572**

INTERNATIONAL APPLICATION NO.

PCT/CH00/00120

INTERNATIONAL FILING DATE

March 3, 2000

PRIORITY DATE CLAIMED

March 3, 1999

TITLE OF INVENTION

**METHOD AND DEVICE FOR PROCESSING FILAMENT YARN, AND USE OF SAID DEVICE**

APPLICANT(S) FOR DO/EO/US

**Patick BUCHMÜLLER**

Applicant(s) herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☐ This is an express request to begin national examination procedures (35 U.S.C. 371(f)). The submission must include items (5), (6), (9) and (21) indicated below.
4. ☒ The US has been elected by the expiration of 19 months from the priority date (Article 31).
5. ☒ A copy of the International Application as filed (35 U.S.C. 371 (c)(2)).
  - a. ☐ is attached hereto (required only if not communicated by the International Bureau).
  - b. ☒ has been communicated by the International Bureau.
  - c. ☐ is not required, as the application was filed with the United States Receiving Office (RO/US).
6. ☒ An English language translation of the International Application as filed (35 U.S.C. 371 (c)(2)).
  - a. ☒ is attached hereto.
  - b. ☐ has been previously submitted under 35 U.S.C. 154 (d)(4).
7. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371 (c)(3)).
  - a. ☐ are attached hereto (required only if not communicated by the International Bureau).
  - b. ☐ have been communicated by the International Bureau.
  - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
  - d. ☒ have not been made and will not be made.
8. ☐ An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371 (c)(3)).
9. ☐ An oath or declaration of the inventor(s) (35 U.S.C. 371 (c)(4)).
10. ☒ An English language translation of the annexes of the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371 (c)(5)).

**Items 11 to 20 below concern document(s) or information included:**

11. ☐ Information Disclosure Statement under 37 CFR 1.97 and 1.98
12. ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. ☐ A **FIRST** preliminary amendment.
14. ☐ A **SECOND** or **SUBSEQUENT** preliminary amendment.
15. ☐ A Substitute specification.
16. ☐ A change of power of attorney and/or address letter.
17. ☐ A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821-1.825.
18. ☐ A second copy of the published international application under 35 U.S.C. 154 (d)(4).
19. ☐ A second copy of the English language translation of the international application 35 U.S.C. 154 (d)(4).
20. ☒ Other items or information:
  - a. ☒ Copy of cover page of International Publication No. WO00/52240
  - b. ☐ Copy of Notification of Missing Requirements.
  - c. ☒ Preliminary Remarks

PCT/CH00/00120

a. ☒ A check in the amount of \$ 1130.00 to cover the above fees is enclosed.

b. ☐ Please charge my Deposit Account No. \_\_\_\_\_ in the amount of \$ \_\_\_\_\_ to cover the above fees.  
A duplicate copy of this sheet is enclosed.

c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to  
Deposit Account No. 06-0916. A duplicate copy of this sheet is enclosed.

d. ☐ Fees are to be charged to a credit card. **WARNING:** Information on this form may become public. **Credit card  
information should not be included on this form.** Provide credit card information and authorization on PTO-2038.

PATENT  
Customer No. 22,852  
Attorney Docket No. 06074.0020

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Application National Stage )  
Application of PCT/CH00/00120 )  
Application No.: Unknown ) Group Art Unit: Unknown  
Filed: Herewith ) Examiner: Unknown  
For: METHOD AND DEVICE FOR )  
PROCESSING FILAMENT YARN, )  
AND USE OF SAID DEVICE )

Assistant Commissioner for Patents  
Washington, DC 20231

Sir:

**PRELIMINARY REMARKS**

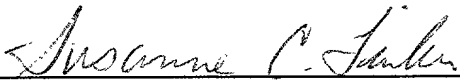
Prior to the examination of the above application, Applicant would like to draw the Examiner's attention to the English translations of the above-referenced international application being submitted herewith. The English translations of the international application include a translation of the originally-filed pages of the international application and a translation of revised pages filed in the international application. These revised pages are referred to in and form the basis of the International Preliminary Examination Report dated April 18, 2001, corresponding to the international application. The specification pages marked as "REVISED PAGE" replace all of the originally-filed specification pages of the international application, and thus constitute the entire international application specification on which the present national stage application is based. Additionally, the drawing sheet labeled "Revised Page" and containing Figs. 3a-3c should replace the originally-filed drawing sheet containing Figs.

3a-3c. Thus, in examining this national stage application, the Examiner should refer to the revised pages instead of the originally-filed pages where such revised pages exist. Should the Examiner have any questions regarding these remarks and the English translations filed herewith, the Examiner is invited to telephone the undersigned at (202) 408-4445.

Respectfully submitted,

FINNEGAN, HENDERSON, FARABOW,  
GARRETT & DUNNER, L.L.P.

Dated:

By:   
Susanne C. Tinker  
Reg. No. 44,472

LAW OFFICES

FINNEGAN, HENDERSON,  
FARABOW, GARRETT,  
& DUNNER, L.L.P.  
1300 I STREET, N. W.  
WASHINGTON, DC 20005  
202-408-4000

8/pts

09/914572

518 Rec'd PCT/PTO 31 AUG 2001

Translated from the German – Rush Translations

Ruth Boggs Translations, Tel.: 703.378.9305, Fax: 703.378.1624, Email: [REZB@aol.com](mailto:REZB@aol.com)

WO 00/52240

PCT/CH00/00120

**Method and Device for Treatment of Filament Yarn  
and Use of Said Device**

**Technical scope**

This invention relates to a method and a device for treatment of filament yarn in a yarn channel of a nozzle with a supply of blowing medium into the yarn channel.

**State of the art**

Treatment of continuous filament yarn has mainly two functions. First, a textile character and technical textile properties are to be imparted to the yarn which is produced from filaments synthesized industrially. Secondly, the yarn is treated from the standpoint of specific quality features for further processing and/or for the end product. To some extent, grades of yarn must be manufactured that are not necessary and cannot be achieved with products produced from natural fibers. The fields of application are in industrial processing of textiles, e.g., for the construction sector, the automotive sector as well as for carpet production and for special textile products for use in the sports and leisure industries. Furthermore, spun yarn is to be treated for the best possible industrial processing by applying of certain preparations, and the processing operation is to be optimized for yarns and fabrics. Optimization in this sense also includes maintaining or increasing certain quality criteria and lowering production costs, which includes downtime along the entire processing route.

Various treatments such as preparation and finishing of yarn by way of yarn treatment nozzles are an important part of filament spinning. The change in structure from a smooth yarn to a textured or interlaced yarn is achieved by means of mechanical air forces. In the case of texturing, a textile character is to be imparted to the smooth yarn. Small loops in the filaments are produced with a supersonic flow, and thus a greater volume is achieved over the entire yarn. In interlacing, knots are formed in the yarn at short intervals, increasing cohesion of the yarn and imparting more stable running of the yarn in processing and in spooling. Air treatment nozzles are used to improve the structure of a yarn. One very demanding process is the improvement in quality by treatment with superheated steam, e.g., for relaxing a yarn as part of a drawing operation or after a previous process measure. In all cases, the nozzle bodies are made of a highly wear-resistant material, because otherwise their lifetime would be too short.

The preparation step is a not insignificant source of problems for yarn treatment nozzles. In this process, yarn is provided with protective substances immediately after the spinning operation or after production of individual filaments. These protective substances should be of assistance in subsequent processing. The substances used for this preparation step result in an oily lubricant property, so that the sliding friction of the yarn remains as low as possible over the entire path of processing, the risk of damage and yarn breakage is reduced, and abrasion on the friction surfaces of the conveyance and processing installations can be minimized. However, there are a number of other factors such as static charge buildup on which the preparation or preparation agent can have a positive influence. Another field of application is for protection of yarn from fungal attack during storage times between the various processing stages.

The drawing operation is another very important process step for filament yarn. After filaments leave the spinnerets, the yarns formed from them must be drawn. This drawing presupposes that the yarn is more or less smooth, although that is no longer the case when processing a textured yarn. In a great many applications, there is a need for imparting a minimal interconnection to the yarn. However, this interconnection may only be intense enough so that it does not have a negative effect on downstream processing operations. It is known that an intermingling nozzle can be arranged downstream from the site of application of preparation agents in a spinning operation. In this case, only very weak knots are formed in the yarn, or even better, only the beginnings of knots are formed to stabilize the transport operations which follow directly. One disadvantage here is finding optimum conditions or an optimum compromise between no knots at all and just the beginnings of knots. The intermingling nozzles known so far are characterized by poor utilization of the air treatment or a weak eddy formation, especially with a relatively low pressure of the processing air. In practice, the uniformity and constancy of the resulting yarn structure often suffer. In the state of the art there is no stable yarn treatment option or a corresponding device which produces enough filament interconnection that calm and stable yarn running is assured without any negative effects on downstream procedures, structural changes or process stages.

### **Explanation of the invention**

The object of this invention was to develop a method as well as yarn treatment nozzles which would permit prebonding of the yarn interconnection, in particular with the greatest possible constancy of a gentle structural operation. The goal was to produce the interconnection even at the highest speeds of yarn transport, e.g., at speeds of 3000-7000 m/min, directly downstream



Translated from the German – Rush Translations

Ruth Boggs Translations, Tel.: 703.378.9305, Fax: 703.378.1624, Email: [REZB@aol.com](mailto:REZB@aol.com)

WO 00/52240

PCT/CH00/00120

from the spinnerets and in direct conjunction with the application of preparation agents. Part of the object of this invention was in particular to improve the situation for treatment of yarn from the standpoint of preparation agents, productivity, especially quality, even at the highest speeds.

The method according to this invention is characterized in that the blowing medium is introduced into the yarn channel in the direction of thread passage at an angle of introduction with a deviation of greater than  $15^\circ$  from the perpendicular to the direction of thread travel, and the preparation agent is added to the yarn directly before the introduction of the blowing medium, or it may be added through the blowing medium itself.

The device according to this invention is characterized in that it is designed as a migration nozzle having a compressed air feed channel into the yarn channel, said compressed air feed channel being aimed in the direction of yarn travel and arranged in the yarn channel with a deviation greater than  $15^\circ$  from a perpendicular to the direction of yarn travel.

This invention also relates to the use of this device for thorough mixing and uniform distribution of preparation agents on filament yarn, whereby the filaments are joined to form a slightly crossed but knot-free yarn, and the preparation agent is at the same time distributed optimally over the entire yarn.

This invention permits a large number of especially advantageous embodiments. In this regard, reference is made to claims 2 through 10 and 12 through 16.

Practice has shown that with an increase in yarn transport speed, namely to more than 3500 m/min in the case of polyester, for example, more than 3000 m/min in the case of polypropylene and more than 4200 m/min in the case of polyamide, thread running becomes unstable and erratic despite the preparation. This instability increases further with any further increase in spinning yarn speed. This becomes problematical in the case of higher multi-end spinning positions. This is true in particular of deflection rollers and drawing rollers in pre-oriented POY and finished-oriented FOY as well as fully drawn FDY spinning operations. Another factor is that a progressively smaller separation [between yarn runs] is desired, not least of all for reasons pertaining to mechanical engineering and the process technology, so that with the same machine depth which would previously accommodate four yarn runs, the desired goal today is eight to ten. With a smaller separation, there is an increased risk of skipping of filaments from

adjacent yarn runs, which could then immediately cause a thread break. Not least of all for ecological reasons but also for economic reasons, it is impossible to increase the application of preparation agents to an unlimited extent through contact with the preparation lips accordingly.

All experiments so far have shown that the range up to 15° represents a barrier for the angle of introduction of blowing air into the yarn channel or on the longitudinal middle axis LM of an intermingling nozzle. In most cases the air jet is directed at right angles onto the longitudinal middle axis in the case of intermingling nozzles, to produce two uniform eddies in the yarn channel. All experience so far has shown that the greater the inclination of the direction of the blowing air, e.g., in the range of about 10° to approximately 15° to a perpendicular line with respect to the yarn run, the greater the conveyance component of the air and thus the more the intermingling nozzle will lose its actual function, namely that of producing intermingling knots. Therefore, in those cases in which a certain air treatment was sought in the manner of the intermingling nozzles but without forming knots in the yarn, it seemed obvious to use an intermingling nozzle from the state of the art but to simply lower the air pressure until, for lack of energy, the compressed air could no longer form knots. One disadvantage of this was that the reproducibility of the results left much to be desired.

Systematic experimental series with this novel invention have surprisingly shown that new effects occur with a suitable adjustment of the blowing air pressure in the range of angles of introduction of more than 15°, namely there is a slight crossing of filaments with a corresponding mixing effect. The actual surprise found in our own experiments was that in the case of prior application of preparation agent to the yarn, this preparation agent would be optimally distributed on the yarn or the individual filaments and in particular the effect of the preparation agent would be significantly greater even with a reduction of 5% to 20% in the amount of preparation agent in comparison with the known practice. Smooth running, stability and a greater operating reliability can be achieved with this new solution. Thus, in many cases this makes it possible to save on preparation agent in the amount of 10-20% or more. There are many possible applications. It was very soon found that the effect of slight crossing would not interfere with any of the downstream treatment stages, e.g., neither drawing nor production of a knotted yarn or thermal effects such as relaxation would cause any interference. This novel invention thus fulfills a double function for use of the preparation agent, namely crossing and optimizing the application and distribution of the preparation agent. Due to the fact a strong conveyance effect is imparted to the air stream in the direction of yarn travel, it is possible not only to increase the yarn transport speed but also to increase the effect of the air in the sense of

creating intense air eddies without producing knots. This therefore makes available for actual practice a novel element having some very positive effects that were not possible in this way in the past and it permits a variety of possible applications. In the majority of application cases, air is the optimum blowing medium. However, it has been found that steam can also be used as the medium in special applications, e.g., for relaxation. This novel process step is referred to below as the migration step, and the novel air nozzle is referred to as the migration nozzle.

In POY and FOY/FDY spinning operations, the thread run is calmer with an additional migration step. There is a stabilizing effect of the thread on the downstream deflection rollers or drawing rollers, not least of all due to the more uniform distribution of spinning preparation between the filaments and thus also due to compensation of differences in thread tension. This takes place as described below, depending on the spinning operation:

- In the FOY/FDY process, the thread is stabilized on the drawing rollers and the deflection rollers due to a more uniform distribution of the spinning preparation in the thread and a slight mingling of the filaments (a type of continuous intermingling without knotting). There must not be any intermingling points, because they would lead to differences in friction on the drawing rollers in the drawing operation. The migration nozzle is located upstream from the first drawing roller. If intermingling is necessary, it is performed upstream from the spooler with an additional air intermingling nozzle.
- In the POY process, the goal is also stabilization of the thread on the rollers (deflection rollers here) through a more uniform distribution of spinning preparation between the filaments. The installation position is the same.
- In the BCF process, individual filaments in the yarn are stabilized and the preparation is distributed. In the tricolor process, a slight color separation in the yarn is also achieved. The installation position is the same as that with the other processes.

The stream of blowing air is preferably produced with compressed air of less than 6 bar, preferably less than 1.5 bar, especially preferably from 0.3 bar to 1.2 bar. In the case of finer yarns, a pressure of approximately 0.5 bar has proven to be optimum. By means of the migration nozzle, a new method which was not known in previous practice is implemented with the crossing of the filaments. The most proximate art is intermingling. In intermingling, a

blending and interconnection of the individual filaments of a yarn is sought; this can be discerned by visible knots in the product. In migration, no knots should be formed; this is achieved on the one hand by an angle of introduction of more than  $15^\circ$ , preferably  $20^\circ$  to  $60^\circ$ , especially less than  $45^\circ$ , and on the other hand also with a lower pressure of the treatment air. Instead of forming knots, only a blending and crossing of the filaments are desired. The stream of air aimed in the direction of yarn travel has a sufficiently intense distribution and mixing function for the preparation agent in the yarn channel. The preparation agent is distributed much more uniformly over the entire yarn by means of the eddy current and the very intense movement of filaments relative to one another due to local whirling and frictional movements of the filaments, resulting in an obviously more stable thread running with a very good interconnection effect for the filaments of a yarn, even at the highest yarn conveyance speeds in effect today. The above-mentioned skipping effect was no longer detected after use of this novel invention, so that the risk of thread breakage can be reduced significantly. Treatment in the migration nozzle as part of the spinning operation preferably takes place immediately after preparation at very high yarn transport speeds.

The migration nozzle has a continuous treatment channel which widens in the direction of thread running in many applications, with a supply of compressed air aimed into the yarn channel in the direction of transport, opening into the yarn channel with a deviation of more than  $15^\circ$  from a perpendicular line. The migration nozzle is arranged at a free distance directly downstream from a device for applying preparation agents. The effective yarn channel length is preferably designed so that it widens steadily, with the smallest cross section being in the area of the yarn feed and the largest cross section being in the area of the yarn draw-off from the yarn channel of the migration nozzle. Experiments so far have shown that good results are achieved when the ratio of the inlet cross section to the outlet cross section is approximately 1:2. The air feed opens approximately at the end of the first third of the treatment channel. The migration nozzle preferably has a threading slot over the length of the yarn channel, preferably arranged in the upper third of the yarn channel in the plane of separation between the nozzle plate and the baffle plate. The migration nozzle may be designed as a single nozzle, a double nozzle or a multiple nozzle.

Instead of the migration [nozzle], the same nozzle or a slightly modified nozzle may also be used for relaxation, in which case steam is required instead of compressed air. Depending on the application, the nozzle may be used as a closed nozzle or as an open nozzle having a threading slot.

The inventors have recognized the fact that a nozzle with connecting means remains reliable in operation only if the nozzle can withstand pressure, heat, steam and chemicals. Not all problems encountered in practice have been solved satisfactorily with the glue joints used in the past. Glue joints can also be investigated only inasmuch as the practical connections are already known. However, the composition of a glue joint cannot be stipulated with regard to attack by as yet unknown chemicals to be used in the future, not to mention the additional effects of heat and moisture. Preferably the connecting means in the novel solution are arranged in the same alignment, preferably aligned so they are flush with the yarn travel. It has surprisingly been found with a corresponding pin connection that the entire nozzle body can be designed to be much smaller, even in miniaturized form in comparison with the state of the art. Especially in the case of use of a double nozzle or multiple nozzles side by side, the separation between two adjacent yarn runs can be selected to be much smaller than in the past. In some applications, this even has a feedback effect on the size of the godet rollers. Due to the possibility of miniaturization, additional yarn runs can be provided on the same machine size, thanks to this novel connection, and the total output of the machine can be increased accordingly. This means that the connection means which is otherwise used in clock and watch technology brings unexpected advantages in an entirely different area. The forced cohesion of the parts can be ensured by a traditional screw connection, as in the state of the art. This novel embodiment is especially advantageous in the application as an intermingling nozzle and as a thermal treatment body, and it is very advantageous when used as a migration nozzle, as will be explained below.

In agreement with the known intermingling nozzles, the treatment medium is directed at the longitudinal center axis of the yarn channel with the greatest possible accuracy, but with an inclination of more than 15° in the yarn transport direction. This produces uniform eddies on both sides but no knots.

### **Brief description of the invention**

This novel invention is explained below on the basis of several embodiments with additional details, showing in great enlargement:

Figure 1: a preparation with a migration nozzle connected to it, each shown in a sectional view;

Figure 2a: the migration nozzle from Figure 1 on a larger scale;

Figure 2b: the air intermingling flow in the yarn channel;

Figure 2c: a single migration nozzle and

Figure 2d: a double migration nozzle as an open structural design with a threading slot;

Figures 3a-3c: an optimum connection of a divided nozzle with alignment pins;

Figures 4a and 4b: two migration nozzles having different opening angles  $\beta$  of the yarn channel;

Figures 5a-5c: various embodiments of a migration nozzle having an integrated preparation medium feed;

Figure 6a: an enlargement of the untreated smooth yarn;

Figure 6b: smooth yarn with crossing of the filaments;

Figure 6c: intermingled yarn having two typical knots with a left-hand rotation and a right-hand rotation;

Figures 7a-7c: schematically three different areas of application of a migration nozzle as well as an intermingling nozzle of the state of the art;

Figures 8a and 8b: two examples of POY yarn;

Figures 9a-9c: three fields of application for FDY yarn;

Figure 10a: use in technical grade yarns;

Figure 10b: use for BCF yarn.

### **Methods and execution of the invention**

Figure 1 shows a detail of a yarn treatment stage 1, showing the chemical preparation stage 2 at the left and the migration stage 3 at the right. Yarn 4 comes directly from a spinning operation and passes over a preparation device having a base body 5 in which a feed channel for the preparation agent CH,Pr passes from beneath into the area of the thread running and ends with the so-called preparation lips 7. Two guide webs 8 are arranged in a U shape over the preparation lips 7, guiding yarn 4 laterally over the preparation lips 7. The base body 5 preferably has a cambered guide groove 9 such that the thread running is force-guided over the location of contacting of yarn 4 with preparation agents CH,Pr. Application of the preparation agent CH,Pr to yarn 4 then takes place in the manner of an entrainment effect through sliding contact. Since the preparation agent CH,Pr is under pressure in feed channel 6 only inasmuch as a reliable secondary flow is guaranteed, it is impossible to wet all the filaments of the yarn uniformly. As a result, yarn 4 cannot be finished with preparation agents homogeneously by means of preparation lips 7. Depending on the type of preparation agent, the film of preparation

agent, some of which is applied to only one side, dries rapidly, so its efficacy remains reduced. The present inventors have recognized the fact that this problem can be eliminated according to a first embodiment of this invention by subjecting the yarn 4 to a more intense air eddy current in a migration nozzle 10. A double eddy current flow has proven to be optimal, producing a thorough mixing of the preparation agent in the entire yarn composite and at the same time causing the filaments in thread 4' to be crossed. This should prevent the development of intermingling knots (Figure 6c). The yarn is opened due to the double eddy current and the individual filaments are crossed slightly with respect to each other (see Figure 6b).

A migration nozzle 10 is shown again in a sectional view on a larger scale in Figure 2a. The migration nozzle 10 is designed in two parts and consists of an upper cover plate or baffle plate 11 and a bottom nozzle plate 12 with connection 13 for the treatment medium. The medium is guided from connection 13 through a first borehole 14 and a compressed medium feed channel 15 into the yarn channel 16. The direction of introduction is important here and is designated as the angle  $\alpha$ . The angle  $\alpha$  must be greater than  $10^\circ$  to a perpendicular line with respect to the yarn running in yarn channel 16. According to experiments so far, the angle  $\alpha$  should be even greater than approximately  $15^\circ$ . A double eddy is produced, as was previously the case, by the angle range from  $15^\circ$ - $60^\circ$ , but at the same time a strong conveyance effect in the yarn transport direction is also achieved. As shown in Figure 2a, the mouth of the compressed medium feed channel 15 is located at the end of approximately the first third of the yarn channel 16, as indicated by X and Y. The free cross section of the yarn channel 16 becomes increasingly larger in the yarn transport direction at the three sections marked by the dimension arrows (beginning of treatment channel A, mouth of air injection B and end of treatment channel C). The size of the narrowest cross section will depend on the titer of the yarn, as is already known to be the case with intermingling nozzles. The area F3 is approximately twice as large as F1, depending on the angle, and F2 is proportional between the two values for F1 and F3 accordingly. In contrast with the preparation stage 2 where a chemical preparation agent (ChPr) is supplied, the migration stage 3 works with a gaseous medium. It may be simply compressed air, heated air or steam, depending on the type of treatment intended. A free distance FA between the preparation device 5 and the migration nozzle 10 is a great advantage for the subsequent installation of a migration nozzle in existing installations. The gaseous medium used with the migration nozzle 10 should at least act dominantly in the yarn transport direction so that the gaseous medium is blown back into the entrance area 20 of the yarn channel 16 as little as possible, which could thus interfere with application of the chemical preparation agent Ch.Pr. As mentioned

previously, a relatively low pressure of the treatment gas is needed for migration, and in many applications it may even be approximately 0.3 to 1.5 bar. The baffle face 21 is preferably designed as a flat face, whereas the opposite side 22 (air injection side) is rounded. The width of the channel in the area of the nozzle plate KBD should be at least equal to or greater than the channel width KBP in the baffle plate according to Figure 2b, so that the individual filaments do not stick or catch at the transitions, especially in the area of the threading slot 23, and no corresponding trouble is caused. Figure 2c shows a single yarn treatment nozzle, and Figure 2d shows a double nozzle. The separation T between two adjacent yarn runs is shown in Figure 2d. In many cases it is possible to provide two or more channels which act accordingly instead of just a single compressed medium feed channel 15.

Figures 3a and 3b show a two-part migration nozzle 10 as a sectional view of Figure 3c. Figure 3a shows a section IIIa-IIIa, Figure 3b shows a section IIIb-IIIb of Figure 3c. Figure 3c shows a section III-III of Figure 3a. Migration nozzle 10 consists of a nozzle plate 11 and a cover plate 12. The two parts are rigidly connected by means of a screw 32 (Figure 3b). For accurate positioning, in particular as an assembly aid, nozzle plate 11 and cover plate 12 are each secured with two alignment pins 33, 33' to prevent displacement in a plane (labeled as X-X in Figure 3b) according to arrow 34. The alignment pins 33, 33' shown here have a double function in this example. In addition to positioning the nozzle plate and the cover plate relative to one another, they also serve the function of local fixation of the entire migration nozzle 10 on a mount 35 (not shown). Alignment pins 33, 33' have already been assembled in one of the nozzle parts at the manufacturing plant. It is important here not to rely on a glue connection, a welded connection or a soldered connection but instead the mechanical clamping means yield the required anchoring in the material of the air treatment body. A tension spring or tension ring 36 forms the mechanical clamping means. An undercut of approximately the same shape as the tension means is produced for tension ring 36 adjacent to an insertion cone in the nozzle plate 11. An insertion cone facilitates automatic assembly of the alignment pins. Nozzle plate 11 has two fitting boreholes. The alignment pin can also be inserted by hand into a through-hole 37 (shown with dotted lines) until the tension ring approaches the narrowest passage of the insertion cone. The rest of the movement for insertion of the alignment pin 33 can be accomplished by tapping lightly, e.g., by means of a rubber hammer, so that tension spring 38 springs into the undercut. In the completely assembled state, the alignment pin 33 projects beyond on both sides. The counterpart to nozzle plate 11 is cover plate 12 which has two axially parallel fitting bores at an identical spacing accordingly. The two parts 11, 12 are assembled for the first time at the manufacturing plant. At the user's plant, the parts can be removed in the



axial directions of the alignment pins for cleaning the parts after loosening screw 32, for example. Another great advantage of the invention proposed here is that subsequent recycling is improved due to the ease of separation, and each material can be processed separately. This is important because the yarn treatment nozzles are expendable parts.

Figures 3a and 3c show a possible shape of a yarn channel 16 for treatment of yarn with compressed air or steam, where  $D_L$  marks the location for a connection for supplying a medium, said medium being introduced into yarn channel 16 at 1 to 10 bar, for example through a feed bore 15. The two alignment pins 33, 33' are preferably arranged together with the screw 32 on a common line 37 (VE). This optimizes the fitting connection and the force connection and allows an especially narrow separation for the yarn running.

The two base bodies of the migration nozzles are made of a highly wear-resistant and very expensive material, especially a ceramic. The boreholes or seats for the clamping means can be produced in a standardized or automated operation with regard to the diameters and diameter ratios. However, the alignment pins can be fabricated as inexpensive decotage [sic?] parts in various lengths for the respective application.

Figures 2b, 2c and 2c [sic; 2d?] and 3a through 3c are also examples of a thermal treatment in one or two through-flow chambers, especially for treatment of yarn with superheated steam or hot air without any immediately preceding preparation. Each through-flow chamber has a yarn inlet 38, a yarn outlet 39 and a medium feed opening 15 in the middle area. If the medium is superheated steam, at the very high yarn transport speeds in use today, this will yield the disadvantage of extremely corrosive conditions for the yarn which has been treated at some point previously with preparation agents. What is especially interesting in this example is that the two through-flow chambers or steam chambers have a considerable length dimension which is due to the working process, or it must be determined from one case to the next. As shown in Figures 2b, 2c and 2d, the yarn treatment body has not only one through-flow chamber but instead has two or more through-flow chambers. With this novel embodiment of the connection means, the two chambers can be constructed especially close to one another. If several parallel yarn runs are needed, this is especially advantageous because this makes it possible to keep the separation T between two adjacent yarn runs extremely small. The alignment pin connection and screw connection are preferably produced on a line 37 parallel to the yarn run and are resistant to preparation agents. The medium supplied through feed opening 15 can leave the

through-flow chamber through the yarn inlet 38 and the yarn outlet 39. If only a single treatment position is in use, the quantity of medium is still low and it can flow into the space. However, if multiple steam positions are used in the same room, the steam must be collected from the through chamber and removed, especially when working with superheated steam. Preferably one or more positions are surrounded with a common medium collecting housing. In the case of the thermal treatment, a jet effect should be avoided. Steam may also be supplied through multiple boreholes. It is important to avoid a strong jet effect due to the thermal medium in the thermal treatment, whether the medium is hot air, superheated steam or any hot medium mixture which may also contain preparation agent, for example.

Figures 4a and 4b each show one example of a different angle of widening  $\beta$  of the yarn channel. Figure 4a shows a larger angle  $\beta$  of 5-10°. Figure 4b shows an angle of less than 6°.

Figure 5a illustrates the possibility of a yarn channel having a constant cross section by using two short parallel lines. Figures 5a through 5c show the basic possibility of adding preparation agent Ch.Pr through a feed channel 6 in a migration nozzle. Preparation agent Ch.Pr is fed directly into yarn channel 16 through a fine bore 40. The preparation agent can be applied directly to the running yarn by stripping accordingly as in the case of the preparation lips. Since there is an enormous variety of different types of preparation agents even with regard to consistency, the specific application of preparation agent must be adapted in special cases. Another possibility is illustrated in Figure 5c, where the preparation agent is introduced into the yarn channel through the borehole 40 in the compressed medium feed channel 15. As in the case of using steam as the treatment medium, it may also be necessary in the case of the solutions to this invention illustrated in Figures 5a-5c to use suction in removing the air coming out. One or more pockets 41 may be provided in the area of the boreholes to achieve a more optimal mixing and application of the preparation agent.

Figure 6a shows a great enlargement of a smooth yarn 4, with the individual filaments running approximately parallel in the thread. Parallel bundling of the filaments has the great disadvantage that, first of all, the thread intermingling is very loose, and secondly, individual filaments can easily become detached from the composite and pose problems in processing. Figure 6c shows as a counterpart a knotted yarn produced in a traditional intermingling nozzle.

This shows one knot at the top and one at the bottom, with L indicating a left-hand knot and R indicating a right-hand knot. The knot connection is relatively stable but it can be loosened again by means of strong and repeated jerky pulling on a portion of knotted yarn. Formation of knots presupposes the use of a filament yarn. If the yarn already has half knots and weak knots, then the actual formation of knots in an intermingling nozzle is difficult and is impaired. The novel crossed yarn (Figure 6b) is a yarn pattern between that of the knotted yarn (Figure 6c) and the smooth yarn (Figure 6a). The individual filaments are slightly crossed with respect to one another or, when considered differently, they are blended running in another constellation. Crossing yields a sufficient cohesion so that the composite structure can no longer become loosened in the processing which follows directly. In particular, individual filaments can no longer become separated from the structure. Crossed yarn gives the required security for transport and spooling up or the special treatment stages in subsequent processing as explained below.

Figure 7a shows schematically from top to bottom a spinning line for POY; Figure 7b shows a spinning line for processing of FDY/FOY as a spinning-drawing line, and Figure 7c shows the use with a spinning-draw texturing line for BCF yarn which has spinning 50, a migration stage 51, a drawing stage 52, a texturizing stage 53 and an intermingling stage 54 with a rinsing station 55 at the bottom. In Figure 7a the drawing and texturing stages are omitted, and in Figure 7b only texturing has been omitted in comparison with Figure 7c.

Figures 8a and 8b as well as 9a through 9c show uses of a migration stage 51 in various spinning operations, with 50 indicating the so-called spinneret or the spinning beam with a connected spinning shaft and the incoming airflow, 2 indicates the preparation stage and 60 shows an automatic yarn-cutting device. Upstream from the spooling stage, intermingling is labeled as 54. The migration stage is 3 and the spooling stages 55. In Figures 8a and 8b, DrTw indicates "draw twisting" and DRW indicates "draw winding" which are performed subsequently. Figures 8a and 8b show an application for POY yarn, but Figures 9a and 9c show an application for FDY yarn. HEAT marks the locations where heat is used.

Figure 10a illustrates a process of technical yarn production, and Figure 10b shows a BCF

[illegible][illegible][illegible]

### Patent Claims

1. A method of treating filament yarn in a yarn channel of a nozzle with a supply of blowing medium into the yarn channel especially aimed at the longitudinal center axis of the yarn channel, **characterized in that** the blowing medium is aimed slightly in the thread running direction and is introduced into the yarn channel at an angle of introduction with a deviation from the perpendicular to the thread run direction of more than 15°.
2. The method according to Claim 2, **characterized in that** preparation agent is added to the yarn before the introduction of the blowing medium or it is introduced through the blowing medium itself.
3. The method according to Claim 1 or 2, **characterized in that** the blowing medium, especially blowing air, is introduced before the longitudinal center of the yarn channel, preferably in the first third, and is preferably aimed at the midline of the yarn channel.
4. The method according to one of Claims 1 through 3, **characterized in that** the angle of introduction is greater than 15° but less than 60°, preferably less than 45°.
5. The method according to one of Claims 1 through 4, **characterized in that** the preparation agent is applied directly to the yarn at a distance before or in the blowing medium introduction per se and then mixes the filaments following application of the blowing medium stream in the yarn transport direction and slightly crosses them while at the same time optimally distributing the preparation agent in the yarn.
6. The method according to Claim 5, **characterized in that** the nozzle is arranged at a free distance directly downstream from a device for applying preparation agents, especially preparation lips, or the preparation agent is applied to the yarn through the nozzle.
7. The method according to one of Claims 1 through 4, **characterized in that** the preparation agent is added to the running yarn directly in the yarn channel upstream or downstream from the introduction of the blowing medium.

8. The method according to one of Claims 1 through 4, **characterized in that** the preparation agent is added to the blowing medium feed directly on entrance into the yarn channel or in the feed channel of the blowing air.
9. The method according to one of Claims 1 through 8, **characterized in that** the blowing medium stream is produced with compressed air at less than 6 bar, preferably less than 1.5 bar, especially preferably from 0.3 bar to 1.2 bar, and the angle of introduction into the yarn channel is preferably 15-30°.
10. The method according to Claim 1, **characterized in that** the blowing medium stream is produced with steam having a pressure of 4-10 bar, preferably 6-8 bar, and the angle of introduction into the yarn channel amounts to 25-45°.
11. The method according to one of Claims 1 through 9, **characterized in that** the treatment is performed as part of a filament-spinning operation at appropriately high yarn transport speeds.
12. The device for treatment of filament yarn **characterized in that** the device is designed as a migration nozzle having a compressed medium feed channel into the yarn channel aimed in the direction of yarn running, said feed channel being directed into the yarn channel with a deviation of greater than 15° from a perpendicular line to the yarn running direction or to the longitudinal center axis of the yarn channel.
13. The device according to Claim 12, **characterized in that** the effective yarn channel length in the yarn running direction preferably widens approximately steadily in the amount of 0-10°, preferably 1-5°.
14. The device according to one of Claims 12 or 13, **characterized in that** the migration nozzle is designed in two parts as a nozzle plate and a baffle plate and has a threading slot over the length of the yarn channel, preferably arranged in the plane of separation between the nozzle plate and the baffle plate.
15. The device according to one of Claims 12 through 14, **characterized in that** the migration nozzle is designed as a single nozzle or as a multiple nozzle.
16. The device according to one of Claims 12 through 15, **characterized in that** the migration nozzle has a feed bore for preparation agent directly in the yarn channel or in the compressed

Translated from the German – Rush Translations

Ruth Boggs Translations, Tel.: 703.378.9305, Fax: 703.378.1624, Email: [REZB@aol.com](mailto:REZB@aol.com)

WO 00/52240

PCT/CH00/00120

air feed channel.

17. The device according to one of Claims 12 through 16, **characterized in that** the yarn channel has one or more pockets for the preparation agent arranged on the opposite side from the mouth of the feed bore for the preparation agent.

18. A use of the device for good mixing and uniform distribution of preparation agents on filament yarn, where the filaments are joined to form a slightly crossed but knot-free yarn, and the preparation agent is at the same time optimally distributed over the entire yarn.

[8 pages of illustrations]

WO 00/52240

Translated from the German – Rush Translation 1  
Ruth Boggs Translations, Tel.: 703.378.9305, Fax: 703.378.1624, Email: [REZB@aol.com](mailto:REZB@aol.com)

HLGes175/PCT

EA/oa

3/15/01

**Method and Device for Treatment of Filament Yarn  
and Use of Said Device**

**Technical scope**

This invention relates to a method and a device for treatment of filament yarn in a yarn channel of a nozzle with a supply of blowing medium into the yarn channel.

**State of the art**

Treatment of continuous filament yarn has mainly two functions. First, a textile character and technical textile properties are to be imparted to the yarn which is produced from filaments synthesized industrially. Secondly, the yarn is treated from the standpoint of specific quality features for further processing and/or for the end product. To some extent, grades of yarn must be manufactured that are not necessary and cannot be achieved with products produced from natural fibers. The fields of application are in industrial processing of textiles, e.g., for the construction sector, the automotive sector as well as for carpet production and for special textile products for use in the sports and leisure industries. Furthermore, spun yarn is to be treated for the best possible industrial processing by applying of certain preparations, and the processing operation is to be optimized for yarns and fabrics. Optimization in this sense also includes maintaining or increasing certain quality criteria and lowering production costs, even with respect to downtime along the entire processing route.

Various treatments such as preparation and finishing of yarn by way of yarn treatment nozzles are an important part of filament spinning. The change in structure from a smooth yarn to a textured or interlaced yarn is achieved by means of mechanical air forces. In the case of texturing, a textile character is to be imparted to the smooth yarn. Small loops in the filaments are produced with a supersonic flow, and thus a greater volume is achieved over the entire yarn. In interlacing, knots are formed in the yarn at short intervals, increasing cohesion of the yarn and imparting more stable running of the yarn in processing and in spooling. Air treatment nozzles are used to improve the structure of a yarn. One very demanding process is the improvement in quality by treatment with superheated steam, e.g., for relaxing a yarn as part of



a drawing operation or after a previous process measure. In all cases, the nozzle bodies are made of a highly wear-resistant material, because otherwise their lifetime would be too short. The preparation step is a not insignificant source of problems for yarn treatment nozzles. In this process, yarn is provided with protective substances immediately after the spinning operation or after production of individual filaments. These protective substances should be of assistance in subsequent processing. The substances used for this preparation step result in an oily lubricant property, so that the sliding friction of the yarn remains as low as possible over the entire path of processing, the risk of damage and yarn breakage is reduced, and abrasion on the friction surfaces of the conveyance and processing installations can be minimized. However, there are a number of other factors such as static charge buildup on which the preparation or preparation agent can have a positive influence. Another field of application is for protection of yarn from fungal attack during storage times between the various processing stages.

The drawing operation is another very important process step for filament yarn. After filaments leave the spinnerets, the yarns formed from them must be drawn. This drawing presupposes that the yarn is more or less smooth, although that is no longer the case when processing a textured yarn. In a great many applications, there is a need for imparting a minimal interconnection to the yarn. However, this interconnection may only be intense enough so that it does not have a negative effect on downstream processing operations. It is known that an intermingling nozzle can be arranged downstream from the site of application of preparation agents in a spinning operation. In this case, only very weak knots are formed in the yarn, or even better, only the beginnings of knots are formed to stabilize the transport operations which follow directly. One disadvantage here is finding optimum conditions or an optimum compromise between no knots at all and just the beginnings of knots. The intermingling nozzles known so far are characterized by poor utilization of the air treatment or a weak eddy formation, especially with a relatively low pressure of the processing air. In practice, the uniformity and constancy of the resulting yarn structure often suffer. In the state of the art there is no stable yarn treatment option or a corresponding device which produces enough filament interconnection that calm and stable yarn running is assured without any negative effects on downstream procedures or process stages or with respect to structural changes.

German Patent 41 02 790 describes a special problem in regard to false twist crimping machines and proposes a delivery nozzle. To this end, the delivery air is blown into the nozzle channel at an angle of  $20^\circ$  to the direction of yarn travel, for example. In the case of a delivery effect almost exclusively, the yarn remains almost unchanged. U.S. Patent 4,214,352 proposes a texturing nozzle for production of a looped yarn. An angle of approx.  $45^\circ$  for introduction is mentioned.

## Explanation of the invention

The object of this invention was to develop a method as well as yarn treatment nozzles which would permit prebonding of the yarn interconnection, in particular with the greatest possible constancy of a gentle structural operation. The goal was to produce the interconnection even at the highest speeds of yarn transport, e.g., at speeds of 3000-7000 m/min, directly downstream from the spinnerets and in direct conjunction with the application of preparation agents. Part of the object of this invention was to improve the situation for treatment of yarn from the standpoint of preparation agents, productivity, especially quality, even at the highest speeds.

The method according to this invention is characterized in that the blowing medium is directed into the yarn channel somewhat in the direction of thread travel and at an angle of introduction with an angle deviation  $\alpha$  from the perpendicular to the direction of thread travel, said angle deviation being greater than 15° but less than 45°, with the filaments of the prepared yarn being blended and slightly crossed without producing knots.

The device according to this invention is characterized in that the device is designed as a migration nozzle having a compressed air feed channel into the yarn channel, said compressed air feed channel being aimed in the direction of yarn travel and arranged in the yarn channel with an angle deviation greater than 15° but less than 45° from a perpendicular to the direction of yarn travel.

This invention also relates to the use of this device for thorough mixing and uniform distribution of preparation agents on filament yarn, whereby the filaments are joined to form a slightly crossed but knot-free yarn, and the preparation agent is at the same time distributed optimally over the entire yarn.

This invention permits a large number of especially advantageous embodiments. In this regard, reference is made to claims 2 through 10 and 12 through 16.

Practice has shown that with an increase in yarn transport speed, namely to more than 3500 m/min in the case of polyester, for example, more than 3000 m/min in the case of polypropylene and more than 4200 m/min in the case of polyamide, thread running becomes unstable and erratic despite the preparation. This instability increases further with any further increase in spinning yarn speed. This becomes problematical in the case of higher multi-end spinning positions. This is true in particular of deflection rollers and drawing rollers in pre-oriented POY

and finished-oriented FOY as well as fully drawn FDY spinning operations. Another factor is that a progressively smaller separation [between yarn runs] is desired, not least of all for reasons pertaining to mechanical engineering and the process technology, so that with the same machine depth which would previously accommodate four yarn runs, the desired goal today is eight to ten. With a smaller separation, there is an increased risk of skipping of filaments from adjacent yarn runs, which could then immediately cause a thread break. Not least of all for ecological reasons but also for economic reasons, it is impossible to increase the application of preparation agents to an unlimited extent through contact with the preparation lips accordingly.

All experiments so far have shown that the range up to  $15^\circ$  represents a barrier for the angle of introduction of blowing air into the yarn channel or on the longitudinal middle axis LM of an intermingling nozzle. In most cases the air jet is directed at right angles onto the longitudinal middle axis in the case of intermingling nozzles, to produce two uniform eddies in the yarn channel. All experience so far has shown that the greater the inclination of the direction of the blowing air, e.g., in the range of about  $10^\circ$  to approximately  $15^\circ$  to a perpendicular line with respect to the yarn run, the greater the conveyance component of the air and thus the more the intermingling nozzle will lose its actual function, namely that of producing intermingling knots. Therefore, in those cases in which a certain air treatment was sought in the manner of the intermingling nozzles but without forming knots in the yarn, it seemed obvious to use an intermingling nozzle from the state of the art but to simply lower the air pressure until, for lack of energy, the compressed air could no longer form knots. One disadvantage of this was that the reproducibility of the results left much to be desired.

Systematic experimental series with this novel invention have surprisingly shown that new effects occur with a suitable adjustment of the blowing air pressure in the range of angles of introduction of more than  $15^\circ$ , namely there is a slight crossing of filaments with a corresponding mixing effect. The actual surprise found in our own experiments was that in the case of prior application of preparation agent to the yarn, this preparation agent would be optimally distributed on the yarn or the individual filaments and in particular the effect of the preparation agent would be significantly greater even with a reduction of 5% to 20% in the amount of preparation agent in comparison with the known practice. Smooth running, stability and a greater operating reliability can be achieved with this new solution. Thus, in many cases this makes it possible to save on preparation agent in the amount of 10-20% or more. There are many possible applications. It was very soon found that the effect of slight crossing would not interfere with any of the downstream treatment stages, e.g., neither drawing nor production of a knotted yarn or thermal effects such as relaxation would cause any interference. This novel

invention thus fulfills a double function for use of the preparation agent, namely crossing and optimizing the application and distribution of the preparation agent. Due to the fact a strong conveyance effect is imparted to the air stream in the direction of yarn travel, it is possible not only to increase the yarn transport speed but also to increase the effect of the air in the sense of creating intense air eddies without producing knots. This therefore makes available for actual practice a novel element having some very positive effects that were not possible in this way in the past and it permits a variety of possible applications. In the predominant majority of application cases, air is the optimum blowing medium. However, it has been found that steam can also be used as the medium in special applications, e.g., for relaxation. This novel process step is referred to below as the migration step, and the novel air nozzle is referred to as the migration nozzle.

In POY and FOY/FDY spinning operations, the thread run is calmer with an additional migration step. There is a stabilizing effect of the thread on the downstream deflection rollers or drawing rollers, not least of all due to the more uniform distribution of spinning preparation between the filaments and thus also due to compensation of differences in thread tension. This takes place as described below, depending on the spinning operation:

- In the FOY/FDY process, the thread is stabilized on the drawing rollers and the deflection rollers due to a more uniform distribution of the spinning preparation in the thread and a slight mingling of the filaments (a type of continuous intermingling without knotting). There must not be any intermingling points, because they would lead to differences in friction on the drawing rollers in the drawing operation. The migration nozzle is located upstream from the first drawing roller. If intermingling is necessary, it is performed upstream from the spooler with an additional air intermingling nozzle.
- In the POY process, the goal is also stabilization of the thread on the rollers (deflection rollers here) through a more uniform distribution of spinning preparation between the filaments. The installation position is the same.
- In the BCF process, individual filaments in the yarn are stabilized and the preparation is distributed. In the tricolor process, a slight color separation in the yarn is also achieved. The installation position is the same as that with the other processes.

The stream of blowing air is preferably produced with compressed air of less than 6 bar, preferably less than 1.5 bar, especially preferably from 0.3 bar to 1.2 bar. In the case of finer

yarns, a pressure of approximately 0.5 bar has proven to be optimum. By means of the migration nozzle, a new method which was not known in previous practice is implemented with the crossing of the filaments. The most proximate art is intermingling. In intermingling, a blending and interconnection of the individual filaments of a yarn is sought; this can be discerned by visible knots in the product. In migration, no knots should be formed; this is achieved on the one hand by an angle of introduction of more than  $15^\circ$ , preferably  $20^\circ$  to  $60^\circ$ , especially less than  $45^\circ$ , and on the other hand also with a lower pressure of the treatment air. Instead of forming knots, only a blending and crossing of the filaments are desired. The stream of air aimed in the direction of yarn travel has a sufficiently intense distribution and mixing function for the preparation agent in the yarn channel. The preparation agent is distributed much more uniformly over the entire yarn by means of the eddy current and the very intense movement of filaments relative to one another due to local whirling and frictional movements of the filaments, resulting in an obviously more stable thread running with a very good interconnection effect for the filaments of a yarn, even at the highest yarn conveyance speeds in effect today. The above-mentioned skipping effect was no longer detected after use of this novel invention, so that the risk of thread breakage can be reduced significantly. Treatment in the migration nozzle as part of the spinning operation preferably takes place immediately after preparation at very high yarn transport speeds.

The migration nozzle has a continuous treatment channel which widens in the direction of thread running in many applications, with a supply of compressed air aimed into the yarn channel in the direction of transport, opening into the yarn channel with a deviation of more than  $15^\circ$  from a perpendicular line. The migration nozzle is arranged at a free distance directly downstream from a device for applying preparation agents. The effective yarn channel length is preferably designed so that it widens steadily, with the smallest cross section being in the area of the yarn feed and the largest cross section being in the area of the yarn draw-off from the yarn channel of the migration nozzle. Experiments so far have shown that good results are achieved when the ratio of the inlet cross section to the outlet cross section is approximately 1:2. The air feed opens approximately at the end of the first third of the treatment channel. The migration nozzle preferably has a threading slot over the length of the yarn channel, preferably arranged in the upper third of the yarn channel in the plane of separation between the nozzle plate and the baffle plate. The migration nozzle may be designed as a single nozzle, a double nozzle or a multiple nozzle.

Instead of the migration [nozzle], the same nozzle or a slightly modified nozzle may also be used for relaxation, in which case steam is required instead of compressed air. Depending on the application, the nozzle may be used as a closed nozzle or as an open nozzle having a

threading slot.

The inventors have recognized the fact that a nozzle with connecting means remains reliable in operation only if the nozzle can withstand pressure, heat, steam and chemicals. Not all problems encountered in practice have been solved satisfactorily with the glue joints used in the past. Glue joints can also be investigated only inasmuch as the practical connections are already known. However, the composition of a glue joint cannot be stipulated with regard to attack by as yet unknown chemicals to be used in the future, not to mention the additional effects of heat and moisture. Preferably the connecting means in the novel solution are arranged in the same alignment, preferably aligned so they are flush with the yarn travel. It has surprisingly been found with a corresponding pin connection that the entire nozzle body can be designed to be much smaller, even in miniaturized form in comparison with the state of the art. Especially in the case of use of a double nozzle or multiple nozzles side by side, the separation between two adjacent yarn runs can be selected to be much smaller than in the past. In some applications, this even has a feedback effect on the size of the godet rollers. Due to the possibility of miniaturization, additional yarn runs can be provided on the same machine size, thanks to this novel connection, and the total output of the machine can be increased accordingly. This means that the connection means which is otherwise used in clock and watch technology brings unexpected advantages in an entirely different area. The forced cohesion of the parts can be ensured by a traditional screw connection, as in the state of the art. This novel embodiment is especially advantageous in the application as an intermingling nozzle and as a thermal treatment body, and it is very advantageous when used as a migration nozzle, as will be explained below.

In agreement with the known intermingling nozzles, the treatment medium is directed at the longitudinal center axis of the yarn channel with the greatest possible accuracy, but with an inclination of more than 15° in the yarn transport direction. This produces uniform eddies on both sides but no knots.

#### Brief description of the invention

This novel invention is explained below on the basis of several embodiments with additional details, showing in great enlargement:

Figure 1: a preparation with a migration nozzle connected to it, each shown in a sectional view;  
Figure 2a: the migration nozzle from Figure 1 on a larger scale;

Figure 2b: the air intermingling flow in the yarn channel;

Figure 2c: a single migration nozzle and

Figure 2d: a double migration nozzle as an open structural design with a threading slot;

Figures 3a-3c: an optimum connection of a divided nozzle with alignment pins;

Figures 4a and 4b: two migration nozzles having different opening angles  $\beta$  of the yarn channel;

Figures 5a-5c: various embodiments of a migration nozzle having an integrated preparation medium feed;

Figure 6a: an enlargement of the untreated smooth yarn;

Figure 6b: smooth yarn with crossing of the filaments;

Figure 6c: intermingled yarn having two typical knots with a left-hand rotation and a right-hand rotation;

Figures 7a-7c: schematically three different areas of application of a migration nozzle as well as an intermingling nozzle of the state of the art;

Figures 8a and 8b: two examples of POY yarn;

Figures 9a-9c: three fields of application for FDY yarn;

Figure 10a: use in technical grade yarns;

Figure 10b: use for BCF yarn.

## Methods and execution of the invention

Figure 1 shows a detail of a yarn treatment stage 1, showing the chemical preparation stage 2 at the left and the migration stage 3 at the right. Yarn 4 comes directly from a spinning operation and passes over a preparation device having a base body 5 in which a feed channel for the preparation agent CH,Pr passes from beneath into the area of the thread running and ends with the so-called preparation lips 7. Two guide webs 8 are arranged in a U shape over the preparation lips 7, guiding yarn 4 laterally over the preparation lips 7. The base body 5 preferably has a cambered guide groove 9 such that the thread running is force-guided over the location of contacting of yarn 4 with preparation agents CH,Pr. Application of the preparation agent CH,Pr to yarn 4 then takes place in the manner of an entrainment effect through sliding contact. Since the preparation agent CH,Pr is under pressure in feed channel 6 only inasmuch as a reliable secondary flow is guaranteed, it is impossible to wet all the filaments of the yarn uniformly. As a result, yarn 4 cannot be finished with preparation agents homogeneously by means of preparation lips 7. Depending on the type of preparation agent, the film of preparation agent, some of which is applied to only one side, dries rapidly, so its efficacy remains reduced.

The present inventors have recognized the fact that this problem can be eliminated according to a first embodiment of this invention by subjecting the yarn 4 to a more intense air eddy current in a migration nozzle 10. A double eddy current flow has proven to be optimal, producing a thorough mixing of the preparation agent in the entire yarn composite and at the same time causing the filaments in thread 4' to be crossed. This should prevent the development of intermingling knots (Figure 6c). The yarn is opened due to the double eddy current and the individual filaments are crossed slightly with respect to each other (see Figure 6b).

A migration nozzle 10 is shown again in a sectional view on a larger scale in Figure 2a. The migration nozzle 10 is designed in two parts and consists of an upper cover plate or baffle plate 11 and a bottom nozzle plate 12 with connection 13 for the treatment medium. The medium is guided from connection 13 through a first borehole 14 and a compressed medium feed channel 15 into the yarn channel 16. The direction of introduction is important here and is designated as the angle  $\alpha$ . The angle  $\alpha$  must be greater than  $10^\circ$  to a perpendicular line with respect to the yarn running in yarn channel 16. According to experiments so far, the angle  $\alpha$  should be even greater than approximately  $15^\circ$ . A double eddy is produced, as was previously the case, by the angle range from  $15^\circ$ - $60^\circ$ , but at the same time a strong conveyance effect in the yarn transport direction is also achieved. As shown in Figure 2a, the mouth of the compressed medium feed channel 15 is located at the end of approximately the first third of the yarn channel 16, as indicated by X and Y. The free cross section of the yarn channel 16 becomes increasingly larger in the yarn transport direction at the three sections marked by the dimension arrows (beginning of treatment channel A, mouth of air injection B and end of treatment channel C). The size of the narrowest cross section will depend on the titer of the yarn, as is already known to be the case with intermingling nozzles. The area F3 is approximately twice as large as F1, depending on the angle, and F2 is proportional between the two values for F1 and F3 accordingly. In contrast with the preparation stage 2 where a chemical preparation agent (ChPr) is supplied, the migration stage 3 works with a gaseous medium. It may be simply compressed air, heated air or steam, depending on the type of treatment intended. A free distance FA between the preparation device 5 and the migration nozzle 10 is a great advantage for the subsequent installation of a migration nozzle in existing installations. The gaseous medium used with the migration nozzle 10 should at least act dominantly in the yarn transport direction so that the gaseous medium is blown back into the entrance area 20 of the yarn channel 16 as little as possible, which could thus interfere with application of the chemical preparation agent Ch.Pr. As mentioned previously, a relatively low pressure of the treatment gas is needed for migration, and in many applications it may even be approximately 0.3 to 1.5 bar. The baffle face 21 is preferably



designed as a flat face, whereas the opposite side 22 (air injection side) is rounded. The width of the channel in the area of the nozzle plate KBD should be at least equal to or greater than the channel width KBP in the baffle plate according to Figure 2b, so that the individual filaments do not stick or catch at the transitions, especially in the area of the threading slot 23, and no corresponding trouble is caused. Figure 2c shows a single yarn treatment nozzle, and Figure 2d shows a double nozzle. The separation T between two adjacent yarn runs is shown in Figure 2d. In many cases it is possible to provide two or more channels which act accordingly instead of just a single compressed medium feed channel 15.

Figures 3a and 3b show a two-part migration nozzle 10 as a sectional view of Figure 3c. Figure 3a shows a section IIIa-IIIa, Figure 3b shows a section IIIb-IIIb of Figure 3c. Figure 3c shows a section III-III of Figure 3a. Migration nozzle 10 consists of a nozzle plate 11 and a cover plate 12. The two parts are rigidly connected by means of a screw 32 (Figure 3b). For accurate positioning, in particular as an assembly aid, nozzle plate 11 and cover plate 12 are each secured with two alignment pins 33, 33' to prevent displacement in a plane (labeled as X-X in Figure 3b) according to arrow 34. The alignment pins 33, 33' shown here have a double function in this example. In addition to positioning the nozzle plate and the cover plate relative to one another, they also serve the function of local fixation of the entire migration nozzle 10 on a mount 35 (not shown). Alignment pins 33, 33' have already been assembled in one of the nozzle parts at the manufacturing plant. It is important here not to rely on a glue connection, a welded connection or a soldered connection but instead the mechanical clamping means yield the required anchoring in the material of the air treatment body. A tension spring or tension ring 36 forms the mechanical clamping means. An undercut of approximately the same shape as the tension means is produced for tension ring 36 adjacent to an insertion cone in the nozzle plate 11. An insertion cone facilitates automatic assembly of the alignment pins. Nozzle plate 11 has two fitting boreholes. The alignment pin can also be inserted by hand into a through-hole 37 (shown with dotted lines) until the tension ring approaches the narrowest passage of the insertion cone. The rest of the movement for insertion of the alignment pin 33 can be accomplished by tapping lightly, e.g., by means of a rubber hammer, so that tension spring 38 springs into the undercut. In the completely assembled state, the alignment pin 33 projects beyond on both sides. The counterpart to nozzle plate 11 is cover plate 12 which has two axially parallel fitting bores at an identical spacing accordingly. The two parts 11, 12 are assembled for the first time at the manufacturing plant. At the user's plant, the parts can be removed in the axial directions of the alignment pins for cleaning the parts after loosening screw 32, for example. Another great advantage of the invention proposed here is that subsequent recycling is improved due to the ease of separation, and each material can be processed separately. This

is important because the yarn treatment nozzles are expendable parts.

Figures 3a and 3c show a possible shape of a yarn channel 16 for treatment of yarn with compressed air or steam, where D<sub>L</sub> marks the location for a connection for supplying a medium, said medium being introduced into yarn channel 16 at 1 to 10 bar, for example through a feed bore 15. The two alignment pins 33, 33' are preferably arranged together with the screw 32 on a common line 37 (VE). This optimizes the fitting connection and the force connection and allows an especially narrow separation for the yarn running.

The two base bodies of the migration nozzles are made of a highly wear-resistant and very expensive material, especially a ceramic. The boreholes or seats for the clamping means can be produced in a standardized or automated operation with regard to the diameters and diameter ratios. However, the alignment pins can be fabricated as inexpensive decotage [sic?] parts in various lengths for the respective application.

Figures 2b, 2c and 2c [sic; 2d?] and 3a through 3c are also examples of a thermal treatment in one or two through-flow chambers, especially for treatment of yarn with superheated steam or hot air without any immediately preceding preparation. Each through-flow chamber has a yarn inlet 38, a yarn outlet 39 and a medium feed opening 15 in the middle area. If the medium is superheated steam, at the very high yarn transport speeds in use today, this will yield the disadvantage of extremely corrosive conditions for the yarn which has been treated at some point previously with preparation agents. What is especially interesting in this example is that the two through-flow chambers or steam chambers have a considerable length dimension which is due to the working process, or it must be determined from one case to the next. As shown in Figures 2b, 2c and 2d, the yarn treatment body has not only one through-flow chamber but instead has two or more through-flow chambers. With this novel embodiment of the connection means, the two chambers can be constructed especially close to one another. If several parallel yarn runs are needed, this is especially advantageous because this makes it possible to keep the separation T between two adjacent yarn runs extremely small. The alignment pin connection and screw connection are preferably produced on a line 37 parallel to the yarn run and are resistant to preparation agents. The medium supplied through feed opening 15 can leave the through-flow chamber through the yarn inlet 38 and the yarn outlet 39. If only a single treatment position is in use, the quantity of medium is still low and it can flow into the space. However, if multiple steam positions are used in the same room, the steam must be collected from the through chamber and removed, especially when working with superheated steam. Preferably

one or more positions are surrounded with a common medium collecting housing. In the case of the thermal treatment, a jet effect should be avoided. Steam may also be supplied through multiple boreholes. It is important to avoid a strong jet effect due to the thermal medium in the thermal treatment, whether the medium is hot air, superheated steam or any hot medium mixture which may also contain preparation agent, for example.

Figures 4a and 4b each show one example of a different angle of widening  $\beta$  of the yarn channel. Figure 4a shows a larger angle  $\beta_2$  of 5-10°. Figure 4b shows an angle of less than 6°. Figure 5a illustrates the possibility of a yarn channel having a constant cross section by using two short parallel lines. Figures 5a through 5c show the basic possibility of adding preparation agent Ch.Pr through a feed channel 6 in a migration nozzle. Preparation agent Ch.Pr is fed directly into yarn channel 16 through a fine bore 40. The preparation agent can be applied directly to the running yarn by stripping accordingly as in the case of the preparation lips. Since there is an enormous variety of different types of preparation agents even with regard to consistency, the specific application of preparation agent must be adapted in special cases. Another possibility is illustrated in Figure 5c, where the preparation agent is introduced into the yarn channel through the borehole 40 in the compressed medium feed channel 15. As in the case of using steam as the treatment medium, it may also be necessary in the case of the solutions to this invention illustrated in Figures 5a-5c to use suction in removing the air coming out. One or more pockets 41 may be provided in the area of the boreholes to achieve a more optimal mixing and application of the preparation agent.

Figure 6a shows a great enlargement of a smooth yarn 4, with the individual filaments running approximately parallel in the thread. Parallel bundling of the filaments has the great disadvantage that, first of all, the thread intermingling is very loose, and secondly, individual filaments can easily become detached from the composite and pose problems in processing. Figure 6c shows as a counterpart a knotted yarn produced in a traditional intermingling nozzle. This shows one knot at the top and one at the bottom, with L indicating a left-hand knot and R indicating a right-hand knot. The knot connection is relatively stable but it can be loosened again by means of strong and repeated jerky pulling on a portion of knotted yarn. Formation of knots presupposes the use of a filament yarn. If the yarn already has half knots and weak knots, then the actual formation of knots in an intermingling nozzle is difficult and is impaired. The novel crossed yarn (Figure 6b) is a yarn pattern between that of the knotted yarn (Figure 6c) and the smooth yarn (Figure 6a). The individual filaments are slightly crossed with respect to one another or, when considered differently, they are blended running in another constellation. Crossing yields a sufficient cohesion so that the composite structure can no longer become loosened in the processing which follows directly. In particular, individual filaments can no

longer become separated from the structure. Crossed yarn gives the required security for transport and spooling up or the special treatment stages in subsequent processing as explained below.

Figure 7a shows schematically from top to bottom a spinning line for POY; Figure 7b shows a spinning line for processing of FDY/FOY as a spinning-drawing line, and Figure 7c shows the use with a spinning-draw texturing line for BCF yarn which has spinning 50, a migration stage 51, a drawing stage 52, a texturizing stage 53 and an intermingling stage 54 with a rinsing station 55 at the bottom. In Figure 7a the drawing and texturing stages are omitted, and in Figure 7b only texturing has been omitted in comparison with Figure 7c.

Figures 8a and 8b as well as 9a through 9c show uses of a migration stage 51 in various spinning operations, with 50 indicating the so-called spinneret or the spinning beam with a connected spinning shaft and the incoming airflow, 2 indicates the preparation stage and 60 shows an automatic yarn-cutting device. Upstream from the spooling stage, intermingling is labeled as 54. The migration stage is 3 and the spooling stages 55. In Figures 8a and 8b, DrTw indicates "draw twisting" and DRW indicates "draw winding" which are performed subsequently. Figures 8a and 8b show an application for POY yarn, but Figures 9a and 9c show an application for FDY yarn. HEAT marks the locations where heat is used.

Figure 10a illustrates a process of technical yarn production, and Figure 10b shows a BCF process.

In Figures 8, 9 and 10, the reference number 60 is shown in parentheses, which should indicate that it is possible to use specifically one migration nozzle alone or a combination with a preparation stage or, as a third possibility, a combined nozzle may be used, e.g., according to Figures 5a-5c.

For the design of the cross-sectional shapes, reference is made to the possibilities according to European Patent 564,400, European Patent 465,407 or U.S. Patent 5,010,631, for example.

HLGes175/PCT

EA/oa

3/15/01

### Patent Claims

1. A migration method of treating filament yarn in a yarn channel 16 of a nozzle with a supply of blowing medium into the yarn channel 16, **characterized in that** the blowing medium is aimed in the thread running direction and is introduced into the yarn channel 16 at an angle of introduction with an angle deviation  $\alpha$  of more than 15° but less than 45° from the perpendicular to the thread run direction, the filaments of the prepared yarn 4, 4' being mixed and slightly crossed without producing knots.
2. The migration method according to Claim 2 [sic; 1], **characterized in that** preparation agent is added to the yarn before the introduction of the blowing medium or it is introduced through the blowing medium itself.
3. The migration method according to one of Claims 1 or 2, **characterized in that** the preparation agent is added to the running yarn 4, 4' directly in the yarn channel 16 upstream or downstream from the point of introduction of the blowing medium.
4. The migration method according to one of Claims 1 through 3, **characterized in that** the preparation agent is added to the blow medium feed directly on entrance into the yarn channel 16 or it is added to the feed channel of the blowing air.
5. The migration method according to one of Claims 1 through 4, **characterized in that** the blowing medium is compressed air at less than 6 bar, which is introduced before the longitudinal center of the yarn channel 16, preferably in the first third, and is aimed at the center line of the yarn channel 16.
6. The migration method according to one of Claims 1 through 5, **characterized in that** the stream of blowing medium is produced with compressed air at less than 1.5 bar and the angle of introduction into the yarn channel 16 is 15° to 30°.
7. The migration method according to Claim 1, **characterized in that** the stream of blowing

medium is produced with steam having a pressure of 4-10 bar, and the angle of introduction into the yarn channel 16 is 25-45°.

8. The migration method according to one of Claims 1 through 7, **characterized in that** the treatment is performed as part of a filament spinning operation at appropriately high transport speeds of the yarn 4.

9. The migration device for treatment of prepared filament yarns, **characterized in that** the device is designed as a migration nozzle 10 having a compressed medium feed channel 15 directed in the direction of yarn travel in the yarn channel 16, said feed channel being aimed into the yarn channel 16 with an angle deviation of greater than 15° but less than 45° from a perpendicular line to the direction of yarn travel or to the longitudinal center axis of the yarn channel 16.

10. The migration device according to Claim 9, **characterized in that** the effective yarn channel length in the yarn running direction preferably widens approximately steadily in the amount of 0-10°, preferably 1-6°.

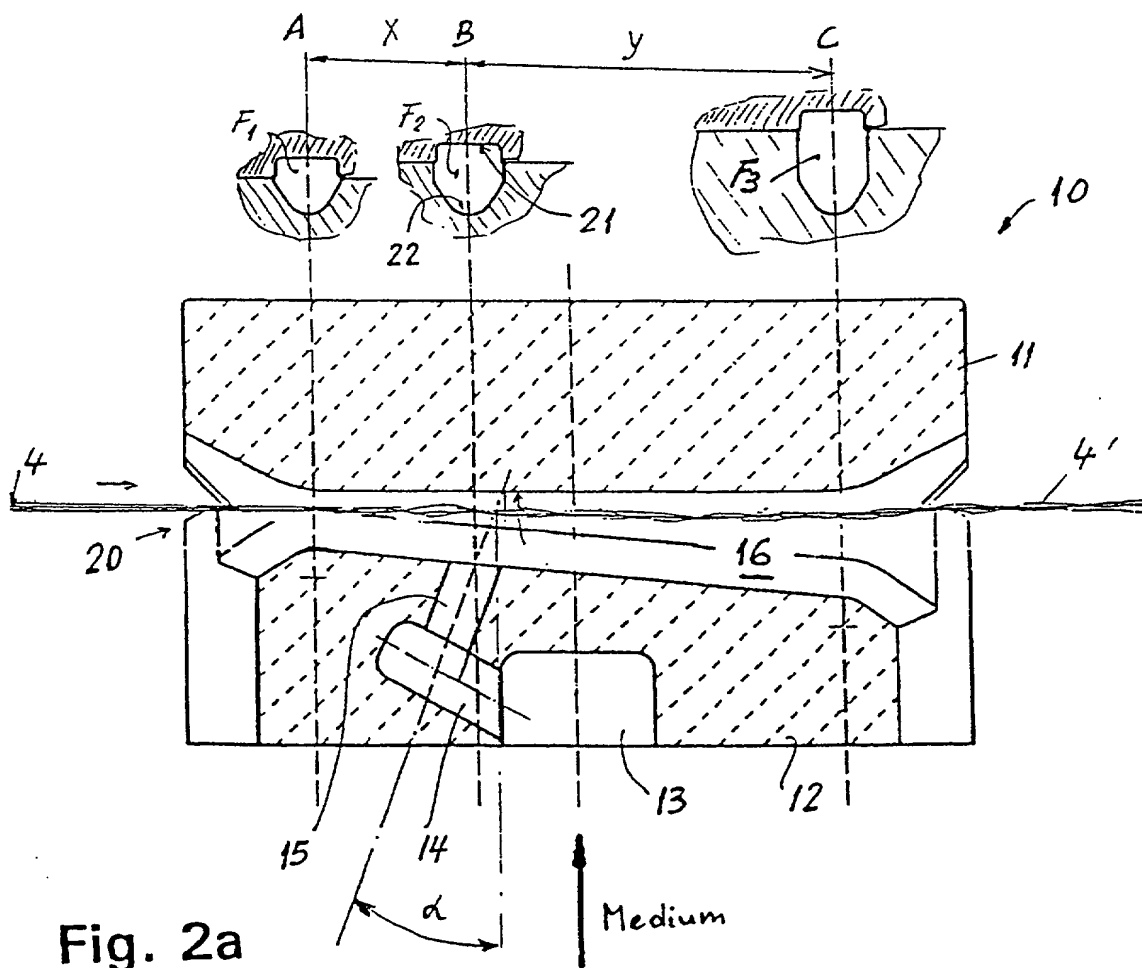
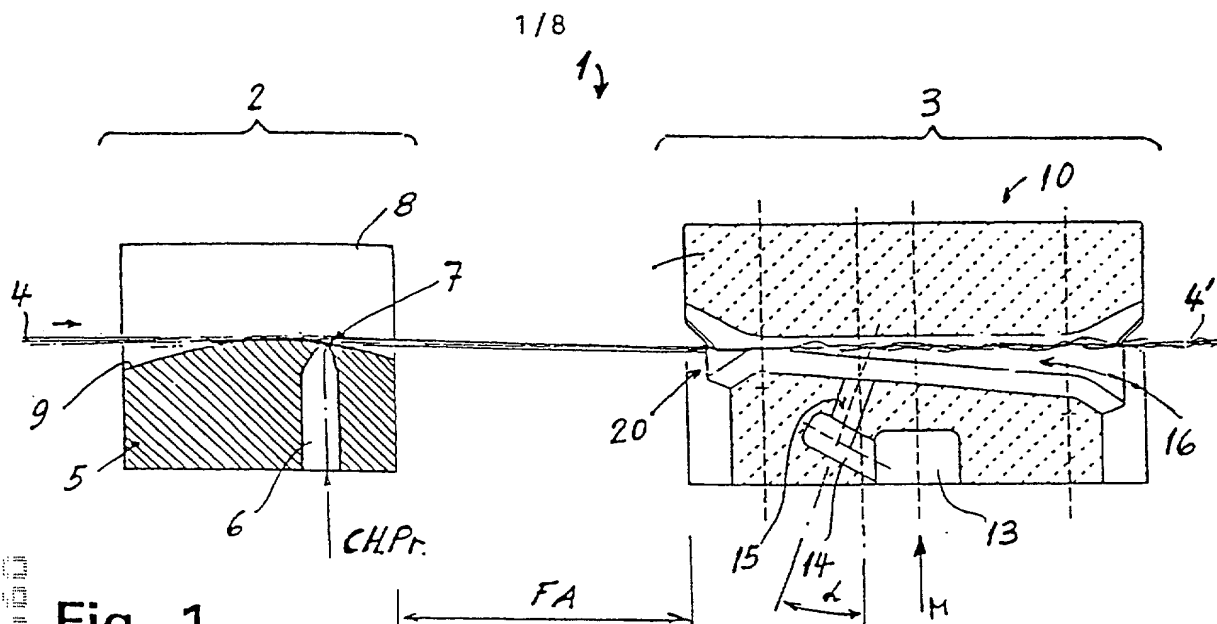
11. The migration device according to one of Claims 9 or 10, **characterized in that** the migration nozzle 10 is designed in two parts as a nozzle plate 12 and a baffle plate 11 and has a threading slot 23 over the length of the yarn channel 16, the slot preferably being arranged in the plane of separation between the nozzle plate 12 and the baffle plate 11.

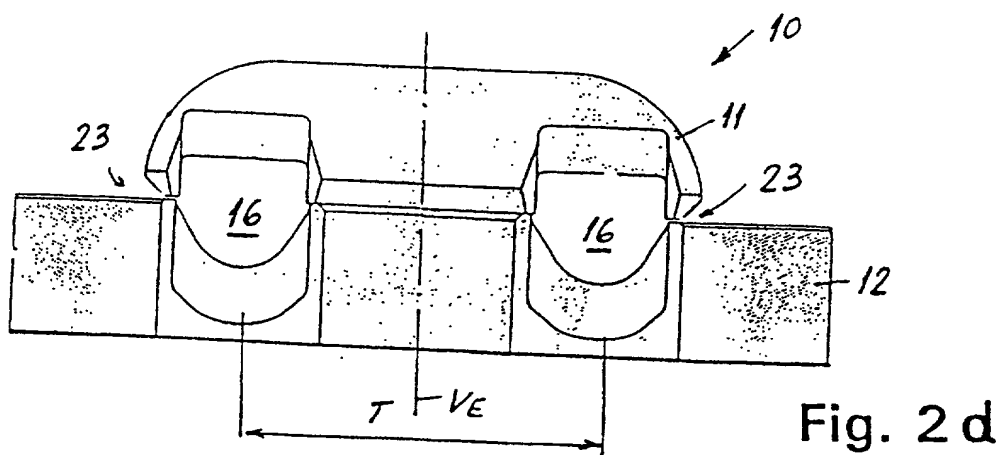
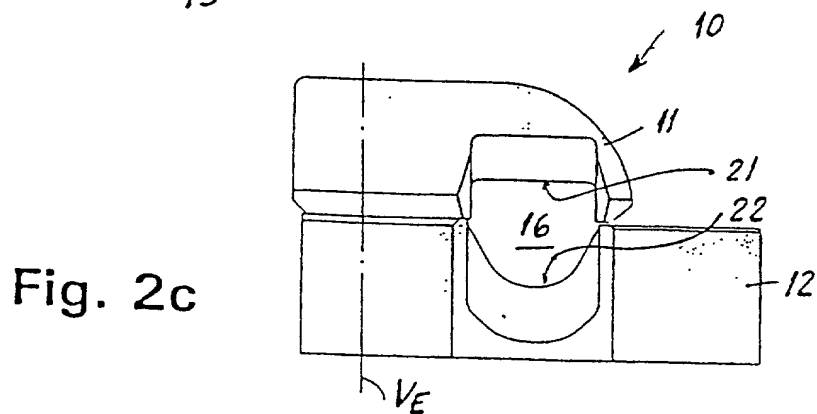
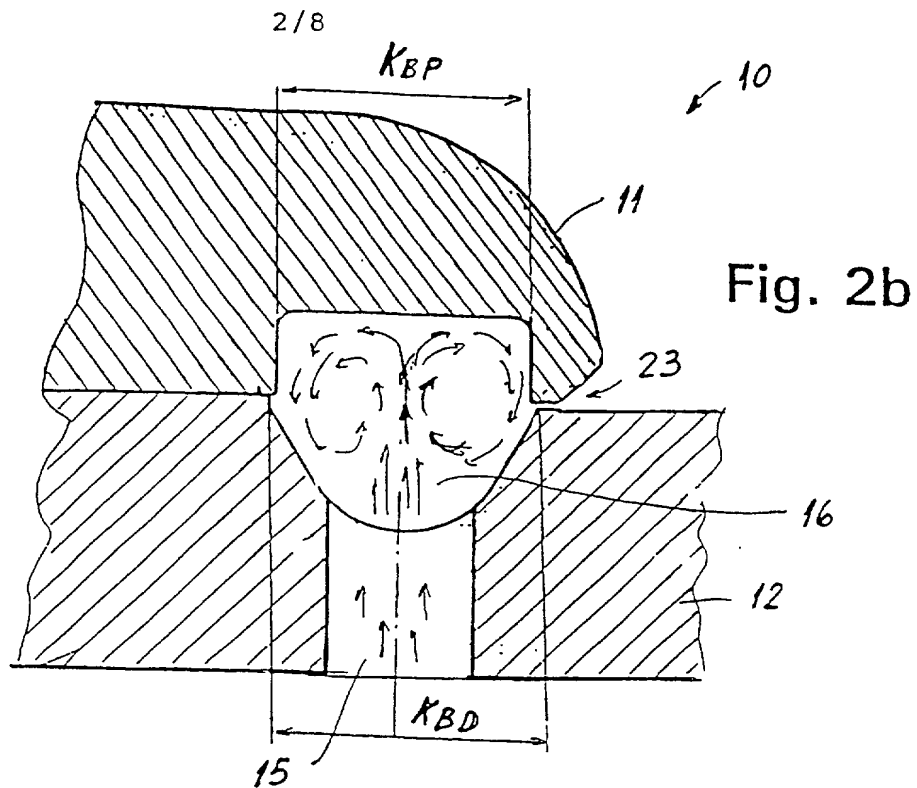
12. The migration device according to one of Claims 9 through 11, **characterized in that** the migration nozzle 10 is designed as a single nozzle or as a multiple nozzle.

13. A device according to one of Claims 9 through 12, **characterized in that** the migration nozzle 10 has a feed bore 40 for preparation agent, directly in the yarn channel 16 or in the compressed air feed channel 15.

14. The device according to one of Claims 9 through 13, **characterized in that** the yarn channel 16 has one or more pockets 41 for the preparation agent arranged on the opposite side from the mouth of the feed bore 40 for the preparation agent.

15. A use of the device for good mixing and uniform distribution of preparation agents on filament yarn, the filaments being joined to form a slightly crossed but knot-free yarn 4, and the preparation agent at the same time being optimally distributed over the entire yarn.







3/8

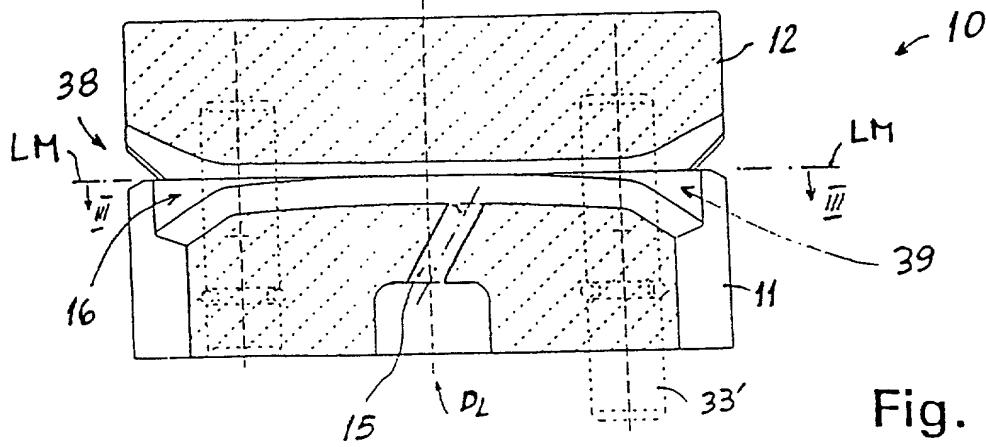


Fig. 3a

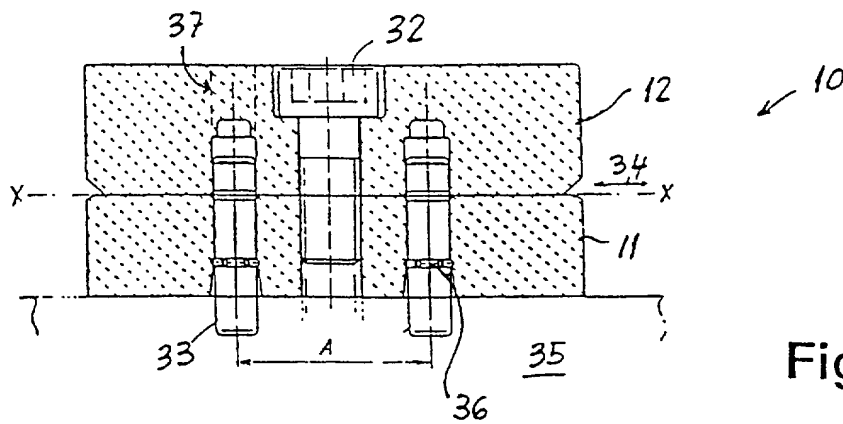


Fig. 3b

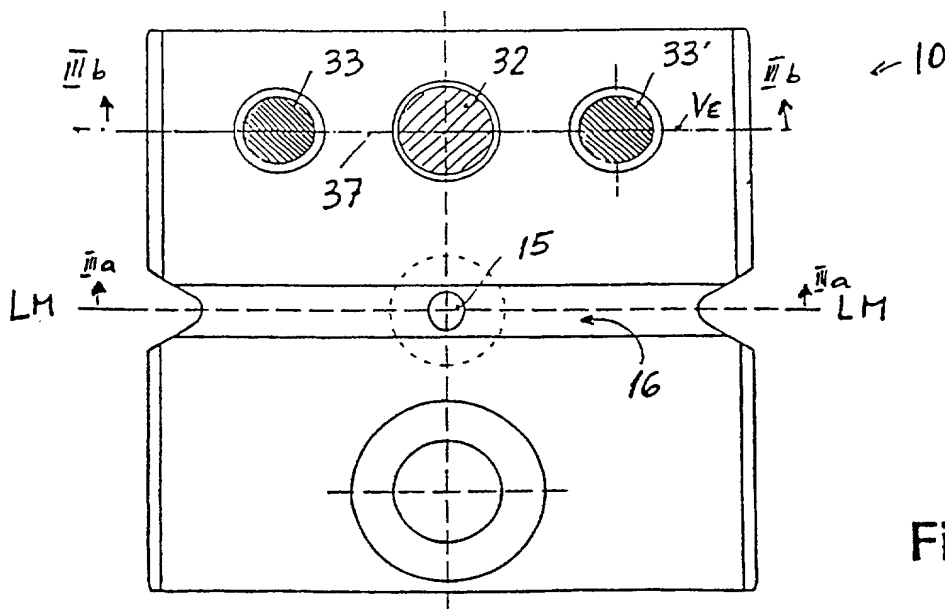


Fig. 3c

4/8

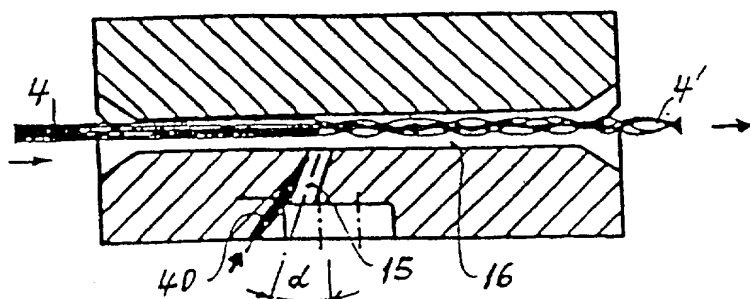


Fig. 5c

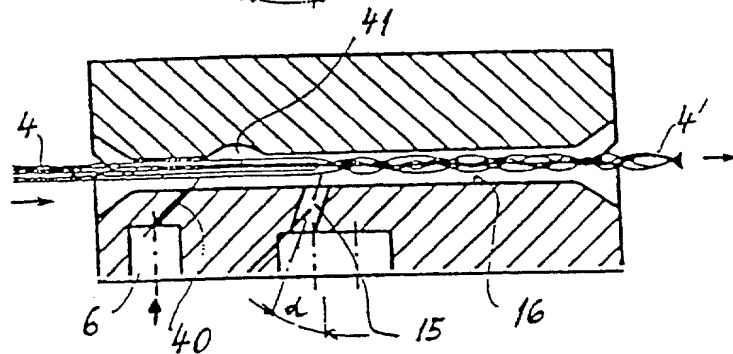


Fig. 5b

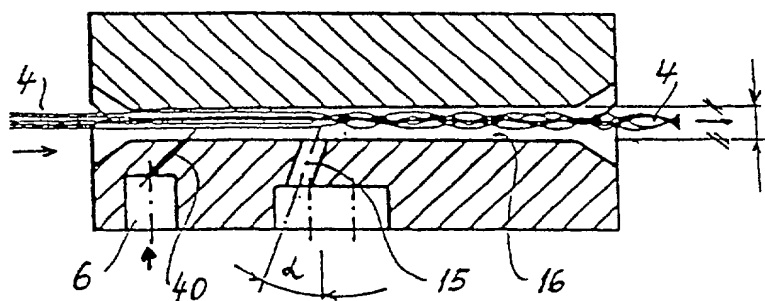


Fig. 5a

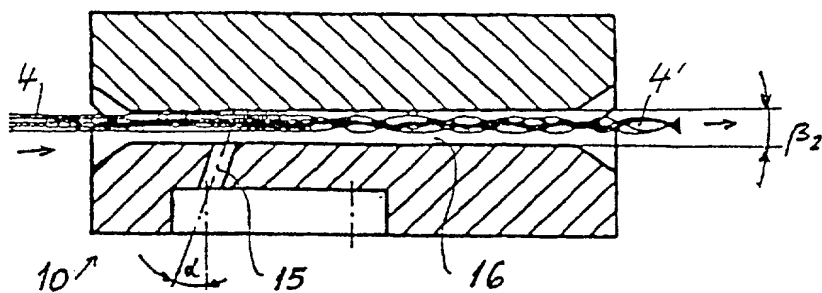


Fig. 4b

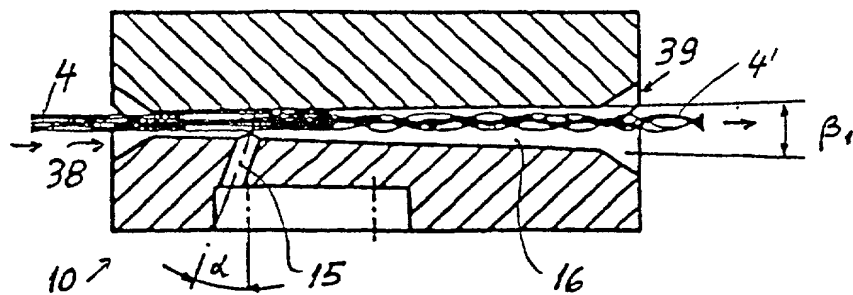


Fig. 4a



**Fig. 6c**

41

→ R

6/8

↓  
POY

↓  
FDY/FOY

↓  
BCF

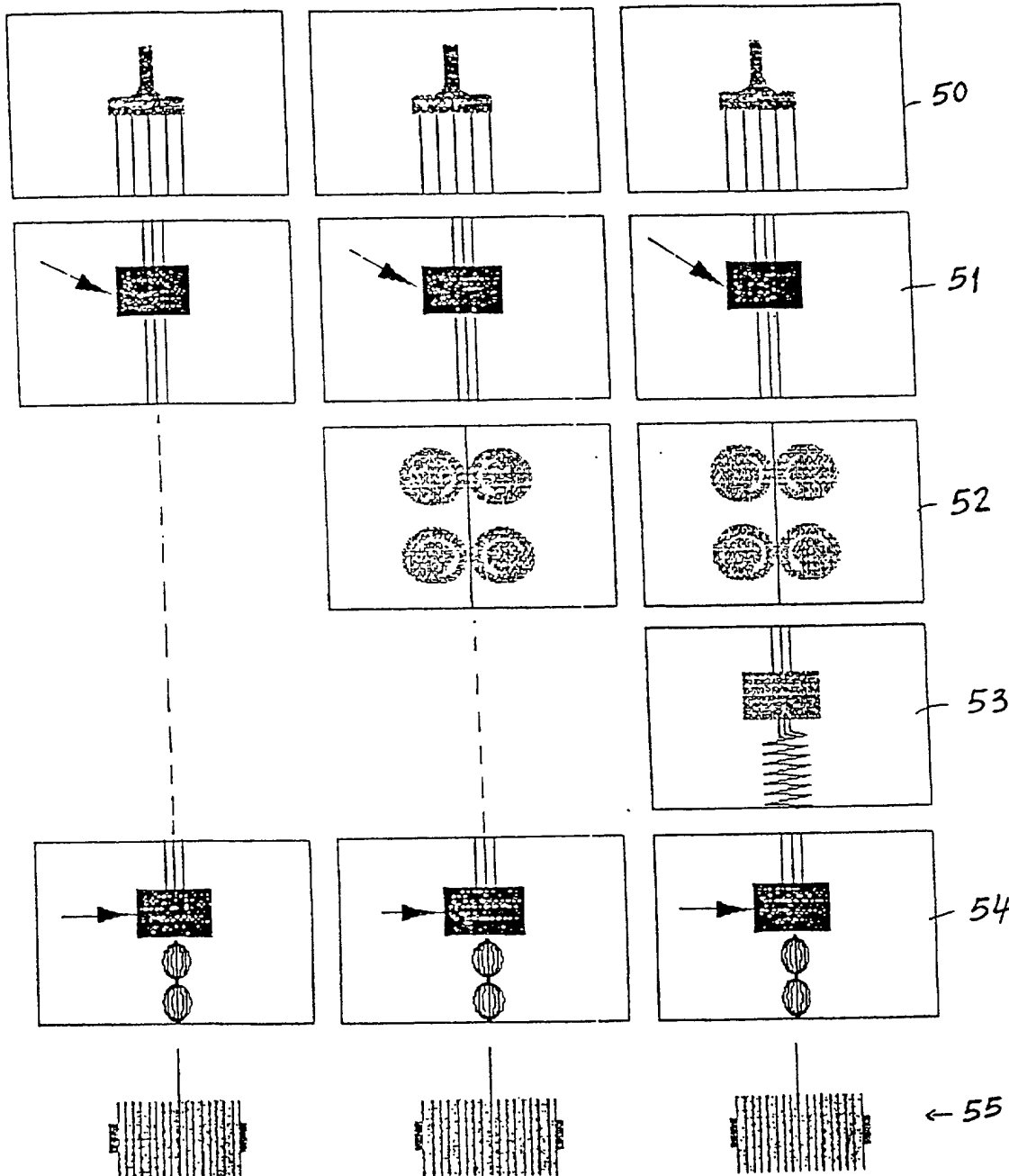


Fig. 7a

Fig. 7b

Fig. 7c

FDY

FDY

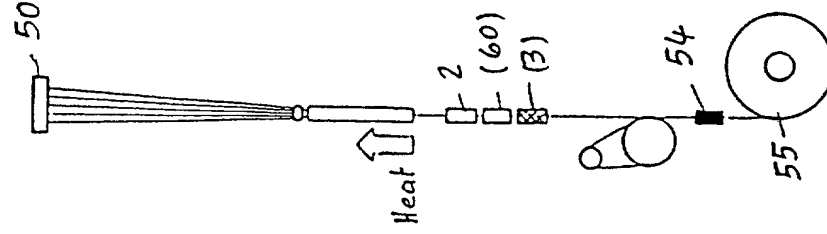
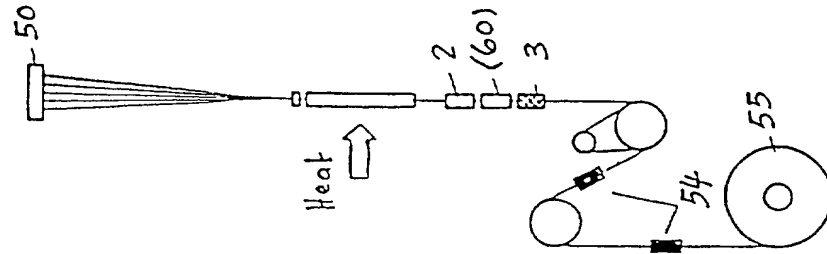
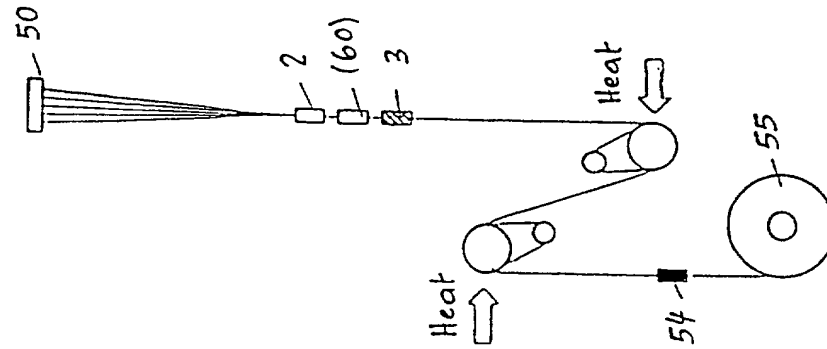
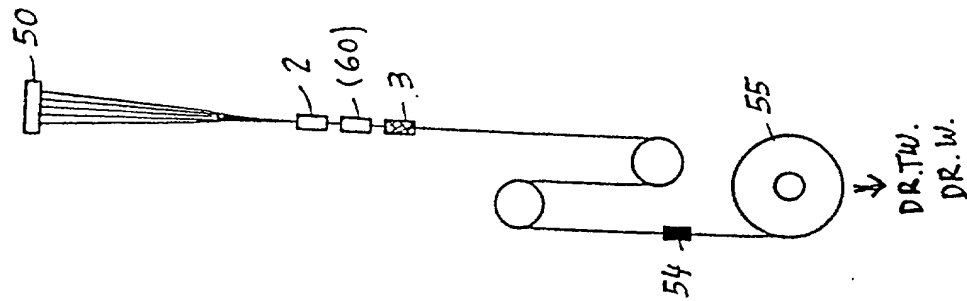
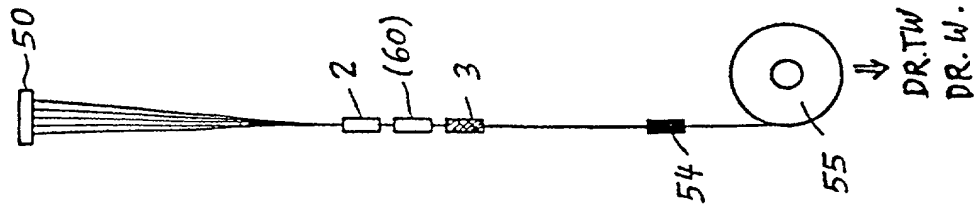
Fig. 8a

Fig. 8b

Fig. 9a

Fig. 9b

Fig. 9c



Techn. Yarn

BCF

Fig. 10a

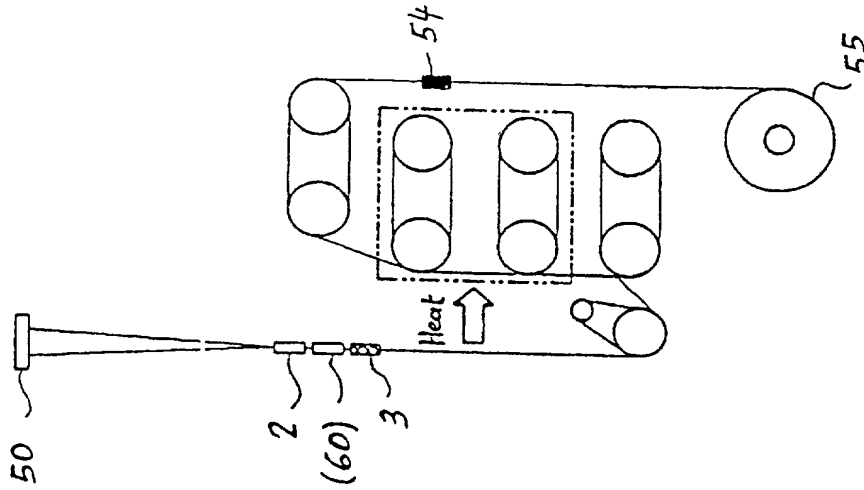
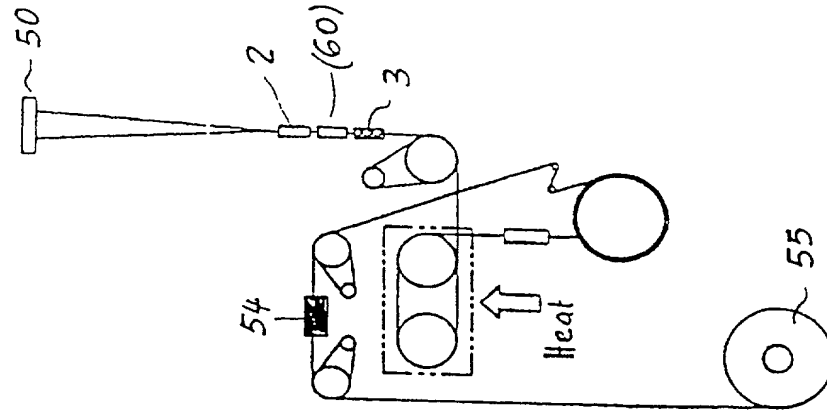


Fig. 10b



## DECLARATION AND POWER OF ATTORNEY

As a below named inventor, I hereby declare that: my residence, post office address and citizenship are as stated below next to my name; I believe I am the original, first, and sole inventor (if only one name is listed below) or an original, first, and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled: **METHOD AND DEVICE FOR PROCESSING FILAMENT YARN, AND USE OF SAID DEVICE** the specification of which ☐ is attached and/or ☒ was filed on August 31, 2001, as United States Application Serial No. \_\_\_\_\_ or on March 3, 2000 as PCT International Application No. PCT/CH00/00120, and was amended on March 15, 2001, (if applicable).

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above. I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR § 1.56.

I hereby claim foreign priority benefits under 35 U.S.C. § 119(a)-(d) or § 365(b) of any foreign application(s) for patent or inventor's certificate or § 365(a) of any PCT international application(s) designating at least one country other than the United States, listed below and have also identified below, any foreign application(s) for patent or inventor's certificate, or any PCT International application(s) having a filing date before that of the application(s) of which priority is claimed:

Country	Application Number	Date of Filing	Priority Claimed Under 35 U.S.C. 119
Switzerland	390/99	March 3, 1999	<input checked="" type="checkbox"/> YES <input type="checkbox"/> NO
			<input type="checkbox"/> YES <input type="checkbox"/> NO

I hereby claim the benefit under 35 U.S.C. § 119(e) of any United States provisional application(s) listed below:

Application Number	Date of Filing

I hereby claim the benefit under 35 U.S.C. § 120 of any United States application(s) or § 365(c) of any PCT International application(s) designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application(s) in the manner provided by the first paragraph of 35 U.S.C. § 112, I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR § 1.56 which became available between the filing date of the prior application(s) and the national or PCT International filing date of this application:

Application Number	Date of Filing	Status (Patented, Pending, Abandoned)

I hereby appoint the following attorney and/or agent(s) to prosecute this application and transact all business in the Patent and Trademark Office connected therewith. **FINNEGAN, HENDERSON, FARABOW, GARRETT & DUNNER, L.L.P.**, Customer Number 22,852, Douglas B. Henderson, Reg. No. 20,291; Ford F. Farabow, Jr., Reg. No. 20,630; Arthur S. Garrett, Reg. No. 20,338; Donald R. Dunner, Reg. No. 19,073; Brian G. Brunsvold, Reg. No. 22,593; Tipton D. Jennings, IV, Reg. No. 20,645; Jerry D. Voight, Reg. No. 23,020; Laurence R. Hefter, Reg. No. 20,827; Kenneth E. Payne, Reg. No. 23,098; Herbert H. Mintz, Reg. No. 26,691; C. Larry O'Rourke, Reg. No. 26,014; Albert J. Santorelli, Reg. No. 22,610; Michael C. Elmer, Reg. No. 25,857; Richard H. Smith, Reg. No. 20,609; Stephen L. Peterson, Reg. No. 26,325; John M. Romary, Reg. No. 26,331; Bruce C. Zotter, Reg. No. 27,680; Dennis P. O'Reilly, Reg. No. 27,932; Allen M. Sokal, Reg. No. 26,695; Robert D. Bajefsky, Reg. No. 25,387; Richard L. Stroup, Reg. No. 28,478; David W. Hill, Reg. No. 28,220; Thomas L. Irving, Reg. No. 28,619; Charles E. Lipsey, Reg. No. 28,165; Thomas W. Winland, Reg. No. 27,605; Basil J. Lewis, Reg. No. 28,818; Martin I. Fuchs, Reg. No. 28,508; E. Robert Yoches, Reg. No. 30,120; Barry W. Graham, Reg. No. 29,924; Susan Haberman Griffen, Reg. No. 30,907; Richard B. Racine, Reg. No. 30,415; Thomas H. Jenkins, Reg. No. 30,857; Robert E. Converse, Jr., Reg. No. 27,432; Clair X. Mullen, Jr., Reg. No. 20,348; Christopher P. Foley, Reg. No. 31,354; John C. Paul, Reg. No. 30,413; Roger D. Taylor, Reg. No. 28,992; David M. Kelly, Reg. No. 30,953; Kenneth J. Meyers, Reg. No. 25,146; Carol P. Einaudi, Reg. No. 32,220; Walter Y. Boyd, Jr., Reg. No. 31,738; Steven M. Anzalone, Reg. No. 32,095; Jean B. Fordis, Reg. No. 32,984; Barbara C. McCurdy, Reg. No. 32,120; James K. Hammond, Reg. No. 31,964; Richard V. Burgujian, Reg. No. 31,744; J. Michael Jakes, Reg. No. 32,824; Thomas W. Banks, Reg. No. 32,719; Christopher P. Isaac, Reg. No. 32,616; Bryan C. Diner, Reg. No. 32,409; M. Paul Barker, Reg. No. 32,013; Andrew Chanho Sonu, Reg. No. 33,457; David S. Forman, Reg. No. 33,694; Vincent P. Kovalick, Reg. No. 32,867; James W. Edmondson, Reg. No. 33,871; Michael R. McGurk, Reg. No. 32,045; Joann M. Neth, Reg. No. 36,363; Gerson S. Panitch, Reg. No. 33,751; Cheri M. Taylor, Reg. No. 33,216; Charles E. Van Horn, Reg. No. 40,266; Linda A. Wadler, Reg. No. 33,218; Jeffrey A. Berkowitz, Reg. No. 36,743; Michael R. Kelly, Reg. No. 33,921; James B. Monroe, Reg. No. 33,971; Doris Johnson Hines, Reg. No. 34,629; Allen R. Jensen, Reg. No. 28,224; Lori Ann Johnson, Reg. No. 34,498; and David A. Manspeizer, Reg. No. 37,540 and \_\_\_\_\_ . Please address all correspondence to **FINNEGAN, HENDERSON, FARABOW, GARRETT & DUNNER, L.L.P.**, 1300 I Street, N.W., Washington, D.C. 20005, Telephone No. (202) 408-4000.

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application or any patent issuing thereon.

Full Name of First Inventor	Inventor's Signature	Date
Patrick BUCHMÜLLER	<i>P Buchmüller</i>	11.10.01
Residence	CHX	Citizenship
Krummenau, Switzerland		Switzerland
Post Office Address	Lütismühle, CH-9643 Krummenan, Switzerland	